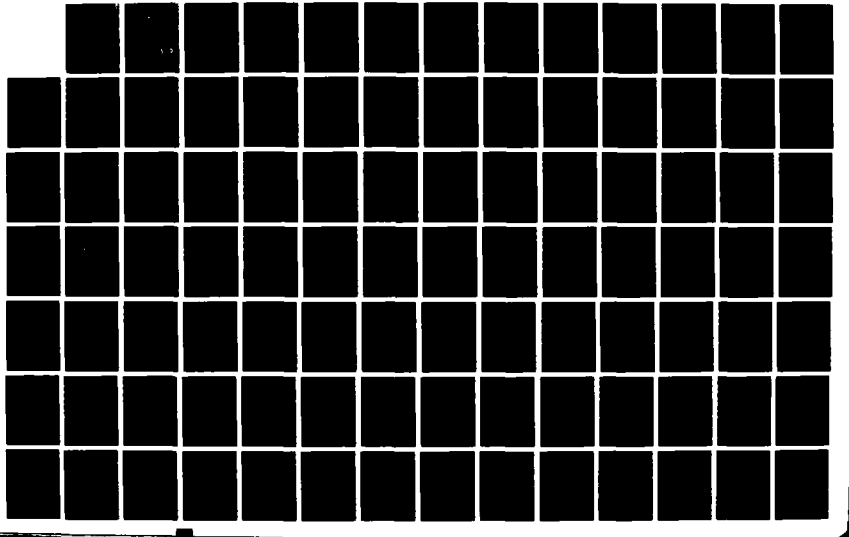
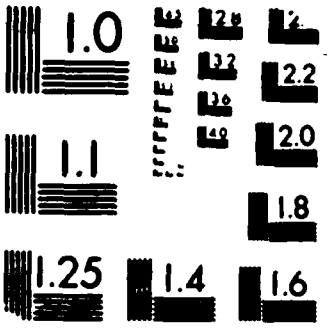
AD-A193 828 F-14 WING OUTER PANEL FATIGUE TEST SPECTRUM(U) NAVAL AIR DEVELOPMENT CENTER WARMINSTER PA AIR VEHICLE AND CREE SYSTEMS TECHN OLOGY DIRECTORATE G S SEIDEL ET AL. 1/3

UNCLASSIFIED APR 87 NADC-87056-60 F/G 1/3.3 NL





MICROCOPY RESOLUTION TEST CHART

(4)

REPORT NO. NADC-87056-60

F-14 WING OUTER PANEL FATIGUE TEST SPECTRUM

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Air Vehicle and Crew Systems Technology Department
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APRIL 1987

FINAL REPORT

Approved for Public Release; Distribution is Unlimited

Prepared for
NAVAL AIR SYSTEMS COMMAND
Department of the Navy
Washington, D.C. 20361-5300

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SECURITY CLASSIFICATION OF THIS PAGE

ADA193828

REPORT DOCUMENTATION PAGE

1a. REPORT SECURITY CLASSIFICATION UNCLASSIFIED	1b RESTRICTIVE MARKINGS N/A
2a. SECURITY CLASSIFICATION AUTHORITY	3. DISTRIBUTION/AVAILABILITY OF REPORT Approved for public release; distribution is unlimited.
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE	
4. PERFORMING ORGANIZATION REPORT NUMBER(S) NADC-87056-60	5. MONITORING ORGANIZATION REPORT NUMBER(S) N/A
6a. NAME OF PERFORMING ORGANIZATION NAVAL AIR DEVELOPMENT CENTER 6b. OFFICE SYMBOL (If applicable) 6041	7a. NAME OF MONITORING ORGANIZATION N/A
6c. ADDRESS (City, State, and ZIP Code) WARMINSTER, PA 18974-5000	7b. ADDRESS (City, State, and ZIP Code) N/A
8a. NAME OF FUNDING/SPONSORING ORGANIZATION NAVAL AIR SYSTEMS COMMAND 8b. OFFICE SYMBOL (If applicable)	9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER N/A
8c. ADDRESS (City, State, and ZIP Code) DEPARTMENT OF THE NAVY WASHINGTON, DC 20361-5300	10. SOURCE OF FUNDING NUMBERS PROGRAM ELEMENT NO: APN-1 / PROJECT NO: - / TASK NO: 241000 749 / WORK UNIT ACCESSION NO: TF670

11 TITLE (Include Security Classification)

F-14 WING OUTER PANEL FATIGUE TEST SPECTRUM

12. PERSONAL AUTHOR(S) G. S. SEIDEL, JR. AND A. KOUTSIOUROUBAS

13a. TYPE OF REPORT	13b. TIME COVERED	14. DATE OF REPORT (Year, Month, Day)	15 PAGE COUNT
FINAL	FROM 1/86 TO 10/86		

16. SUPPLEMENTARY NOTATION

17 COSATI CODES			18 SUBJECT TERMS (Continue on reverse if necessary and identify by block number)
FIELD	GROUP	SUB-GROUP	Aircraft Structure, Fatigue Test
01	03	03	

19. ABSTRACT (Continue on reverse if necessary and identify by block number)

A spectrum of loads for the F-14 Wing Outer Panel fatigue test has been derived, based on the spectrum used by Grumman for the Aircraft #98 test of the F-14A fuselage. Flight and ground load distributions on the wing have been developed corresponding to those in that test, and the Aircraft #98 spectrum was simplified where significant fuselage loading conditions would have negligible effect on the wing outer panel. In addition, requirements for sweeping the wing under load have been incorporated based on fleet operational data.

The Wing Outer Panel Fatigue Test will be performed by Vought Company and it is expected to begin during the third quarter of fiscal year 1988.

20. DISTRIBUTION/AVAILABILITY OF ABSTRACT	21 ABSTRACT SECURITY CLASSIFICATION
☒ UNCLASSIFIED/UNLIMITED ☒ SAME AS RPT ☐ DTIC USERS	UNCLASSIFIED

22a NAME OF RESPONSIBLE INDIVIDUAL	22b TELEPHONE (Include Area Code)	22c OFFICE SYMBOL
G. S. SEIDEL, JR.	(215) 441-2050	Code 6041

DD FORM 1473, 84 MAR 83 APR edition may be used until exhausted. All other editions are obsolete.

SECURITY CLASSIFICATION OF THIS PAGE

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SYMBOLS

B.L. Butt Line (= y)

C.G. Center of Gravity

E Exceedances

F.S. Fuselage Station (= x)

F_x Horizontal Shear ∿ Pounds

F_z Vertical Shear ∿ Pounds

M Mach No.

M_x Moment About x Axis (unswept) ∿ Inch-Pounds

M_y Moment About y Axis (unswept) ∿ Inch -Pounds

M_z Moment About z Axis (unswept) ∿ Inch-Pounds

$M_{x'}$ Moment About x' Axis (WOP axis) ∿ Inch-Pounds

$M_{y'}$ Moment About y' Axis (WOP axis) ∿ Inch-Pounds

N_x Longitudinal Load Factor ∿ g's

N_y Lateral Load Factor ∿ g's

N_z Normal Load Factor ∿ g's

$\dot{p}$ Roll Acceleration ∿ Radians/sec^2

q Dynamic Pressure ∿ Pounds Per Square Foot

W.L. Water Line (= z)

V_{sa} Sinking Speed ∿ Feet Per Second

Λ Wing Leading Edge Sweep Angle ∿ degrees

$\Delta\Lambda$ Change in Sweep Angle ∿ Degrees

V_∞ Free Stream Velocity ∿ Feet Per Second

α Angle of Attack ∿ Degrees

SUMMARY

A spectrum of loads for the F-14 Wing Outer Panel fatigue test has been derived, based on the spectrum used by Grumman for the Aircraft #98 test of the F-14A fuselage. Flight and ground load distributions on the wing have been developed corresponding to those in that test, and the Aircraft #98 spectrum was simplified where significant fuselage loading conditions would have negligible effect on the wing outer panel. In addition, requirements for sweeping the wing under load have been incorporated based on fleet operational data.

INTRODUCTION

A fatigue test is planned, under Naval Air Systems Command (NAVAIR) sponsorship, for the F-14 Wing Outer Panel, including the wing pivot and the structure of the variable sweep panel outboard of the pivot. This part of the F-14 airframe had not been included in the Aircraft #98 fatigue test conducted by Grumman, and so is the remaining structure to be demonstrated to full service lifetime under a realistic flight-by-flight block loading.

AIRCRAFT #98 FATIGUE TEST CONDITIONS

The so-called Aircraft #98 Fatigue Test was conducted by Grumman under NAVAIR Contract beginning in 1977. The purpose of the test was to demonstrate the structural integrity of the fatigue-critical portions of the F-14A airframe, such as the aft fuselage, under a realistic spectrum of loads. The original F-14A fatigue test had undergone many structural beef-ups and spectrum changes in mid-test, so that a re-test to a more complete spectrum representative of actual service operation was required. In addition, modern testing philosophies such as flight-by-flight block loading were incorporated in the Aircraft #98 test. The test article was the fuselage of F-14A shop No. 98, (BUNO 159432) which had sustained damage in a ground accident. The fuselage was repaired and brought to current ECP status by Grumman. The wings were considered less fatigue-critical than the fuselage, and were not included in the test.

It should be noted that since the wing was not included, test loadings were selected based on their criticality to the fuselage. For any given loading condition in the spectrum, the aspects of that condition significant to the fuselage structure were included. Also, only the loads at the wing pivot - shear, moment and torsion - were needed for the Aircraft #98 test; wing outer panel load distributions were not constructed.

Spectrum

The fatigue test spectrum for the Aircraft #98 fatigue test was described in references (a) through (c). The test was intended to demonstrate a fatigue life of 12000 hours. Grumman developed their spectrum in terms of a 480 hour block, a repeatable flight-by-flight sequence with a selected wing sweep schedule. Each 480 hour block consisted of 440 flights. Flight loads consisted of symmetric maneuvers, level rolls, and turn reversals (rolling maneuvers at 3.5 g or greater). The spectrum of flight maneuvers, derived in part from the F-14A Fleet Flight Loads Survey as reported in reference (d), included a breakdown into five wing sweep positions, and a total of 11528 maneuvers per 480 hour block. Of the 440 flights, 160 included carrier takeoffs (catapults) and arrestments. The remaining 280 were field landings and field carrier landing practice (FCLP). Touch-and-go's were included in both carrier and field landings.

Table I, extracted from reference (e), lists the 378 load conditions that made up the Aircraft #98 spectrum. The actual sequential spectrum for a 480 hour block is included in Appendix (A). This spectrum is the one finally applied in the Aircraft #98 test, after some of the lower level loads in the original spectrum were truncated out.

Flight Loads

Derivation of the balanced loads for flight conditions of the aircraft #98 test was documented in reference (b). The contractor measured net loads on a flight test aircraft, extracted airloads from these net loads so as to construct a rational aero model, and then used the aero model and known inertias to develop balanced loads.

A symmetric maneuver load cycle consisted of a peak N_z of 3.5g or greater followed by a valley N_z of less than 1.0g. Wing loads in symmetric maneuvers were found to peak at about 8^o angle of attack. At higher N_z's the additional lift was generated by the fuselage. Therefore, for each wing sweep angle, the peak wing load occurred at a different N_z which was generally lower than the maximum N_z in the spectrum. The aircraft #98 fatigue test load sequence included this peak in the increasing N_z portion of the cycle. A complete symmetric maneuver sequence was as shown below:

$$1.0g \rightarrow \begin{matrix} N_z \text{ for} \\ \text{peak wing} \\ \text{load} \end{matrix} \rightarrow \begin{matrix} \text{Maneuver} \\ N_z \text{ peak} \end{matrix} \rightarrow \begin{matrix} N_z \\ \text{valley} \end{matrix} \rightarrow 1.0g$$

An asymmetric maneuver load cycle consisted of a symmetric N_z condition with an antisymmetric (roll acceleration) component superimposed in each direction sequentially. For a turn reversal, which is an asymmetric maneuver at 3.5g or greater, this sequence was as shown below:

$$1.0g \rightarrow \begin{matrix} \text{Maneuver } N_z \\ +\dot{p} \end{matrix} \rightarrow \begin{matrix} \text{Maneuver } N_z \\ -\dot{p} \end{matrix} \rightarrow \text{Maneuver } N_z \rightarrow \begin{matrix} N_z \\ \text{valley} \end{matrix} \rightarrow 1.0g$$

For level rolls, the maneuver N_z was 1.0g. There were no N_z valleys associated with level rolls.

Ground Loads

Derivation of the balanced loads for ground conditions of the Aircraft #98 test was documented in reference (c). The contractor conducted an extensive series of transient analyses and correlated his model with the results of full scale drop tests and instrumented aircraft landing tests. In the final load sequence, each landing was a function of sinking speed and landing attitude and included up to four cycles of load.

For an arrested landing, the longitudinal loads of the arrestment were considered to follow separately after the vertical loads of the landing.

For a catapult, a sequence of loads including nosing, release, and asymmetric tow loads was applied.

DERIVATION OF WING OUTER PANEL TEST CONDITIONS

The spectrum for the F-14A Wing Outer Panel fatigue test has been derived primarily from the Aircraft #98 test spectrum. In addition, this test is to evaluate the effects of wing sweeping, and so provisions for sweeping the wing under load have been added. Since the Aircraft #98 test wing loads consisted of net loads at the pivot only, a set of distributions has been developed using theoretical aerodynamic analysis. Finally, the Aircraft #98 spectrum has been shortened, primarily in the ground loads area, by simplifying the loading conditions.

The sign conventions used throughout this report are shown in Figure 1. Aircraft #98 test condition loads were derived in an unswept coordinate system for application to the fuselage. However, for this test of the Wing Outer Panel, a coordinate system that remains attached to the wing as it sweeps is useful. Therefore, the wing quarter chord (approximately) line, which passes through the pivot and is at an angle of -3.5° to the leading edge line, is used. This axis system is shown in Figure 1c.

Loads for each test condition consist of pivot location resultants shown in Table II, with distributions that can be constructed from component distributions provided in various other Figures. Wing pivot resultants have five components; no lateral loads are included.

Flight Loads

Derivation of the wing pivot loads for symmetric flight conditions followed the procedures used by Grumman. Table III contains these calculations, and the resulting net pivot loads are considered identical to those that were applied in the Aircraft #98 test. The values of shear, bending moment and torsional moment about unswept axes through the pivot are plotted in Figures 2 through 6 for the various sweep angles. The values of these loads at N_z's other than those calculated were obtained by linear interpolation.

In order to determine the distribution of the airloads over the wing outer panel, a theoretical airloads analysis was performed using the RAPIDLOADS computer code, reference (f). The aerodynamic model of the wing in the 25° sweep position is shown on Figure 7. The model included the effects of camber, twist, dihedral, and fuselage interaction. As with Grumman's Aircraft #98 conditions, no maneuvering flaps or slats were used. The flight conditions for 25° sweep were at Mach 0.62, 10,000 feet altitude. The agreement of this analysis with Grumman's Aircraft #98 data, for the linear region up to an angle of attack $\alpha = 8.2^{\circ}$, can be seen in Figure 8.

Net loads were obtained by combining these airloads with inertia loads. Inertia loads were obtained by constructing a distribution of the 2013 lb empty weight of the wing (for flight maneuvers at the flight design gross weight, there is 50% internal fuel, which is all in the fuselage). For the maximum load condition at 25° sweep, the net loads are as shown in Figure 9.

The loads shown in Tables II and III are in the unswept axis system and in the wing outer panel axis system illustrated in Figures 1b and 1c, respectively. The net loads shown in Figure 9 are located along the Wing Outer Panel quarter chord (Y' axis) illustrated in Figure 1c, rotated into bending and torsion of the quarter chord ($M_{x'}$ and $M_{y'}$ respectively). This figure, therefore, represents a distribution in suitable format for test implementation.

In order to avoid the necessity to derive individual distributions for each flight maneuver condition (which would also complicate the test), an assessment was made of the similarity of these distributions for different N_z and sweep values using Grumman's flight data. Aero data from reference (5) was used to determine the variability of the center of pressure in the axis system that moves with the wing. This variability is shown in Table IV, and illustrated on Figure 10. Inertia load, the other component of the net load distribution, is of course invariant with wing sweep. Therefore, the variation was concluded to be small enough to justify using the same spanwise load distribution for all symmetric flight maneuver load conditions. Scaling the spanwise load distribution will not necessarily match the root torsion value: however, the torsion distribution of Figure 9 should be scaled separately to match the root value.

In the Aircraft #98 test, asymmetric maneuver loads were made up of a symmetric load component, as previously derived, and an antisymmetric component due to rolling acceleration. Since the F-14 uses spoilers and differential tail for roll control instead of ailerons, the additional load in a roll acceleration was considered to come from inertia only. The distributed inertia load due to a unit roll acceleration is shown in Figure 11. This distribution is applicable to both level (1 g) rolls and turn reversals, and can be added to the symmetric load distribution.

Ground Loads

During landing, the wing experiences a reversed loading as it goes from an upward airload to a downward inertia load. The relationship between sinking speed and N_z shown in Figure 12 was used. The wing is considered to be empty of fuel and in the fully forward 20° sweep position. Wing weight is 2019 lb, from reference (g). The unit distribution of inertia load is shown in Figure 13. While the aircraft #98 test used a number of load applications per landing, and a distribution of landing attitudes, for the Wing Outer Panel test only one cycle per landing was assumed, and the acceleration was taken as a function of sinking speed only.

Load factors for arrestment conditions were given in reference (e), and are reproduced here in Table V. The wing was considered to be empty of fuel and positioned at the forward 20° sweep position, the same as for the landing conditions. The inertia load distribution of Figure 13 can be scaled to the proper N_z value and applied in the longitudinal direction.

Catapult conditions were also described in reference (c) and are reproduced here in Table VI. For catapult, the wing was considered to be full of fuel, 2108 lbs per wing, reference (z), and at the 20° sweep position. The unit distribution of inertia load for the full fuel condition is shown in Figure 14. While the Aircraft #98 test used a series of spotting, buffing, tow and release loads to represent a catapult, just one load application per catapult was used for the Wing Outer Panel test.

Spectrum

The Aircraft #98 spectrum in Appendix (A) was modified to produce the F-14 Wing Outer Panel spectrum.

First, simplifications applied to the catapult, landing, and arresting load conditions resulted in deleting some conditions and combining others. Then, any sequential duplications of the same load within a flight were removed. The resulting spectrum is given in Appendix (B), and is available on computer tape. The number of applications of each condition in a 480 hour block is shown on Table II, along with the corresponding number from the original spectrum. Since an asymmetric maneuver involves a sequence of conditions including a symmetric maneuver case, the number of actual maneuvers in the spectrum is not readily apparent from Table II. Table VII, however, gives a summary of the maneuvers included in the spectrum, and the normalized total N_z exceedance curve is plotted in Figure 15.

Pivoting

The amount of wing sweep movement during normal F-14A flight operations was tabulated by Grumman from F-14A Fleet Flight Loads Survey data. The Grumman data is included herein as Table VIII. It is noted that pivoting from forward to aft positions usually occurs during lightly loaded (accelerating in level flight) conditions, while pivoting from aft to forward positions often occurs in higher g maneuvers, when the drag slows the airplane down.

It was decided, for simplicity with no loss of generality, to impose pivoting under load only on the symmetric flight conditions. Each time a symmetric maneuver (N_z = 3.5g or greater) is imposed, a wing pivot cycle will be imposed as described in Figure 16. All pivot cycles will be for 10° except those at $\Lambda_{.25}$ = 25° which will be for 5°. With this test procedure, all ramping up or down of load will occur with the wing stationary, and the number of pivoting movements under load will approximate the total shown in Table VIII for $\Delta\Lambda \geq 5°$.

References:

(a) GAC Report A51-30-R-80-01 (LD 303-110.4): F-14A Fatigue Criteria for Flight Operations for A/C No. 98 Test Program; 9 Feb 80

(b) GAC Report A51-30-R-80-03 (LD 303-102.1): F-14A A/C 98 Fatigue Test Program Balanced Aircraft Flight Loads; 15 Feb 80

(c) GAC Report A51-30-R-80-04: Derivation of Ground Loads for F-14A Aircraft No. 98 Fatigue Test; 15 Apr 80

(d) GAC Report FAD-303-3-3.31: F-14 Fleet Flight Loads Survey Final Report; 16 Nov 79

(e) GAC Report SAR 80-3: 30 Apr 80

(f) NADC-79126-60: PARTLOADS Analysis; 24 Aug 79

(g) GAC Report A51-320-R-78-2; F-14A Aircraft No. 98 Structural Model Test Mass Properties Report

TABLE I Description of Flight and Ground Loading Conditions, Aircraft #98 Fatigue Test

F-14A A.C. 98 FATIGUE CONDITIONS

TRANSIENT RESPONSE NON-ARRESTED COND'S (NO THRUST, WT.=51830LBS)

FATIGUE COND. NO.	MANEUV.	TIME SLICE	SINK SPEED FT/SEC	DESCRIPTION
1	40F	38	26.3	TAIL DOWN SYMMETRIC
2	40F	76	26.3	TAIL DOWN SYMMETRIC
3	40F	142	26.3	TAIL DOWN SYMMETRIC
4	40F	177	26.3	TAIL DOWN SYMMETRIC
5	32F	38	23.0	TAIL DOWN SYMMETRIC
6	32F	72	23.0	TAIL DOWN SYMMETRIC
7	32F	141	23.0	TAIL DOWN SYMMETRIC
8	32F	165	23.0	TAIL DOWN SYMMETRIC
9	39F	34	18.0	TAIL DOWN SYMMETRIC
10	39F	64	18.0	TAIL DOWN SYMMETRIC
11	39F	119	18.0	TAIL DOWN SYMMETRIC
12	39F	165	18.0	TAIL DOWN SYMMETRIC
13	37F	38	14.0	TAIL DOWN SYMMETRIC
14	37F	68	14.0	TAIL DOWN SYMMETRIC
15	37F	118	14.0	TAIL DOWN SYMMETRIC
16	37F	167	14.0	TAIL DOWN SYMMETRIC
17	35F	50	10.0	TAIL DOWN SYMMETRIC
18	35F	197	10.0	TAIL DOWN SYMMETRIC
19	35F	271	10.0	TAIL DOWN SYMMETRIC
20	36F	41	6.0	TAIL DOWN SYMMETRIC
21	36F	174	6.0	TAIL DOWN SYMMETRIC
22	36F	224	6.0	TAIL DOWN SYMMETRIC
23	71F	32	26.3	LEVEL
24	71F	133	26.3	LEVEL
25	71F	165	26.3	LEVEL
26	71F	211	26.3	LEVEL
27	72F	37	23.0	LEVEL
28	72F	158	23.0	LEVEL
29	72F	215	23.0	LEVEL
30	73F	36	18.0	LEVEL
31	73F	148	18.0	LEVEL
32	73F	213	18.0	LEVEL
33	74F	38	14.0	LEVEL
34	74F	152	14.0	LEVEL
35	74F	202	14.0	LEVEL
36	75F	100	10.0	LEVEL
37	75F	233	10.0	LEVEL
38	76F	108	6.0	LEVEL
39	76F	335	6.0	LEVEL
40	81F	28	26.3	TAIL DOWN ROLLED RIGHT
41	81F	67	26.3	TAIL DOWN ROLLED RIGHT
42	81F	93	26.3	TAIL DOWN ROLLED RIGHT
43	81F	139	26.3	TAIL DOWN ROLLED RIGHT
44	82F	22	23.0	TAIL DOWN ROLLED RIGHT
45	82F	69	23.0	TAIL DOWN ROLLED RIGHT
46	82F	90	23.0	TAIL DOWN ROLLED RIGHT

TABLE I Description of Flight and Ground Loading Conditions, Aircraft #98 Fatigue Test (Continued)

47	82F	119	22.0	TAIL DOWN ROLLED RIGHT
48	83F	35	12.0	TAIL DOWN ROLLED RIGHT
49	83F	58	12.0	TAIL DOWN ROLLED RIGHT
50	83F	85	18.0	TAIL DOWN ROLLED RIGHT
51	83F	110	18.0	TAIL DOWN ROLLED RIGHT
52	84F	37	14.0	TAIL DOWN ROLLED RIGHT
53	84F	63	14.0	TAIL DOWN ROLLED RIGHT
54	84F	110	14.0	TAIL DOWN ROLLED RIGHT
55	84F	130	14.0	TAIL DOWN ROLLED RIGHT
56	85F	51	10.0	TAIL DOWN ROLLED RIGHT
57	85F	106	10.0	TAIL DOWN ROLLED RIGHT
58	86F	72	6.0	TAIL DOWN ROLLED RIGHT
59	86F	152	6.0	TAIL DOWN ROLLED RIGHT

RIGID BODY GROUND COND'S

ARRESTED LANDING (THRUST=21920LBS, WT.=53975LBS, 20DEG SWEEP)

FATIGUE COND. NO.	HOOK DRAG LBS	HOOK SIDE LBS	DESCRIPTION
60	171000	27000	SIDE HOOK FORCE TO LEFT
61	171000	16200	SIDE HOOK FORCE TO LEFT
62	159000	27000	SIDE HOOK FORCE TO LEFT
63	159000	16200	SIDE HOOK FORCE TO LEFT
64	148000	27000	SIDE HOOK FORCE TO LEFT
65	148000	16200	SIDE HOOK FORCE TO LEFT
66	171000	-27000	SIDE HOOK FORCE TO RIGHT
67	171000	-16200	SIDE HOOK FORCE TO RIGHT
68	159000	-27000	SIDE HOOK FORCE TO RIGHT
69	159000	-16200	SIDE HOOK FORCE TO RIGHT
70	148000	-27000	SIDE HOOK FORCE TO RIGHT
71	148000	-16200	SIDE HOOK FORCE TO RIGHT

CATAPULT (WT.=71242LBS, 20DEG SWEEP)

FATIGUE COND. NO.	THRUST LBS	TOW LBS	TORQUE IN-LBS	DESCRIPTION
72	21920	237000		SYMMETRIC TOW-LEVEL
73	21920	213000		SYMMETRIC TOW-LEVEL
74	21920	189000		SYMMETRIC TOW-LEVEL
75	21920	237000	260000	SPOT LEFT
76	21920	213000	260000	SPOT LEFT
77	21920	189000	260000	SPOT LEFT
78	21920	237000	-260000	SPOT RIGHT
79	21920	213000	-260000	SPOT RIGHT
80	21920	189000	-260000	SPOT RIGHT
81		-59100		BUFFING
82		-58900		BUFFING
83	21920	-2180		RELEASE

TABLE I Description of Flight and Ground Loading Conditions, Aircraft #98
Fatigue Test (Continued)

UNIT NZ CONDITIONS (BAL. AT FS292 & MAIN GEAR) SWEEP=20

FATIGUE

COND. NO.	DESCRIPTION
84	100(FUEL(16200LBS) ,WT.=63430LBS
85	30(FUEL(4860LBS) ,WT.=52090LBS

FLIGHT CONDITIONS (WT.=56950 LBS)

FATIGUE

COND. NO.	DESIG.	MACH	ALT (FT)	SWEEP (DEG)	NY	NZ	
86	98-01	.620	10000	25	--	-2.250	SYMM
87	98-02	.620	10000	25	--	3.462	SYMM
88	98-03	.620	10000	25	--	5.346	SYMM
89	98-04	.620	10000	25	--	6.943	SYMM
90	98-05	.620	10000	25	--	7.902	SYMM
91	98-06	.620	10000	25	--	8.243	SYMM
92	98-07	.620	10000	25	--	(1)	ANTI
93	98-08	.620	10000	25	--	(3)	ANTI
94	98-09	.703	10000	35	--	-2.250	SYMM
95	98-10	.703	10000	35	--	3.750	SYMM
96	98-11	.703	10000	35	--	6.500	SYMM
97	98-12	.703	10000	35	--	8.123	SYMM
98	98-13	.703	10000	35	--	9.000	SYMM
99	98-14	.703	10000	35	--	(1)	ANTI
100	98-15	.703	10000	35	--	(3)	ANTI
101	98-16	.788	10000	45	--	-2.250	SYMM
102	98-17	.788	10000	45	--	4.272	SYMM
103	98-18	.788	10000	45	--	9.000	SYMM
104	98-19	.788	10000	45	--	(1)	ANTI
105	98-20	.788	10000	45	--	(3)	ANTI
106	98-21	.868	10000	55	--	-2.250	SYMM
107	98-22	.868	10000	55	--	5.068	SYMM
108	98-23	.868	10000	55	--	8.078	SYMM
109	98-24	.868	10000	55	--	9.000	SYMM
110	98-25	.868	10000	55	--	(1)	ANTI
111	98-26	.868	10000	55	--	(3)	ANTI
112	98-27	.975	10000	68	--	-2.253	SYMM
113	98-28	.975	10000	68	--	6.375	SYMM
114	98-29	.975	10000	68	--	9.000	SYMM
115	98-30	.975	10000	68	--	(1)	ANTI
116	98-31	.975	10000	68	--	(3)	ANTI
VOID	117						
VOID**	118						
VOID	119						
VOID	120						
VOID**	121						
VOID	122						

TABLE I Description of Flight and Ground Loading Conditions, Aircraft #98
Fatigue Test (Continued)

FATIGUE COND. NO.							
VOID	123						
	124	9E-02	.620	10000	25	-- 3.460	SYMM
	125	9E-16	.785	10000	45	-- -2.250	SYMM
	126	9E-17	.785	10000	45	-- 4.272	SYMM
	127	9E-27	.975	10000	63	-- -2.253	SYMM
	128	9E-28	.975	10000	68	-- 6.875	SYMM
	129	9E-29	.975	10000	68	-- 9.000	SYMM

* TRANSIENT RESPONSE NON-ARRESTED COND'S (NO THRUST, WT.=51830LBS)

FATIGUE COND. NO.	MANEUV.	TIME SLICE	SINK SPEED FT/SEC	DESCRIPTION
130	81F	28	25.3	TAIL DOWN ROLLED LEFT
131	81F	57	25.3	TAIL DOWN ROLLED LEFT
132	81F	80	25.3	TAIL DOWN ROLLED LEFT
133	81F	106	25.3	TAIL DOWN ROLLED LEFT
134	82F	32	23.0	TAIL DOWN ROLLED LEFT
135	82F	59	23.0	TAIL DOWN ROLLED LEFT
136	82F	80	23.0	TAIL DOWN ROLLED LEFT
137	82F	116	23.0	TAIL DOWN ROLLED LEFT
138	83F	35	18.0	TAIL DOWN ROLLED LEFT
139	83F	58	18.0	TAIL DOWN ROLLED LEFT
140	83F	85	18.0	TAIL DOWN ROLLED LEFT
141	83F	110	18.0	TAIL DOWN ROLLED LEFT
142	84F	37	14.0	TAIL DOWN ROLLED LEFT
143	84F	63	14.0	TAIL DOWN ROLLED LEFT
144	84F	110	14.0	TAIL DOWN ROLLED LEFT
145	84F	130	14.0	TAIL DOWN ROLLED LEFT
146	85F	51	10.0	TAIL DOWN ROLLED LEFT
147	85F	106	10.0	TAIL DOWN ROLLED LEFT
148	86F	73	6.0	TAIL DOWN ROLLED LEFT
149	86F	152	6.0	TAIL DOWN ROLLED LEFT

TABLE I Description of Flight and Ground Loading Conditions, Aircraft #98 Fatigue Test (Continued)

CONDITION NUMBERING

SYMMETRIC FLIGHT

REF n_z	SWEEP ANGLE - DEGREES 25	35	45	55	68
-1.75	150*	165*	180*	195*	210*
-1.25	151	166*	181*	196*	211*
-0.75	152	167	182*	197*	212
-0.25	153	168	183	198	213
0.25	154	169	184	199	214
0.75	155	170	185	200	215
1.00	156	171	186	201	216
3.50	157	172	187	202	217
4.50	158	173	188	203	218
5.50	159	174	189	204	219
6.50	160	175	190	205	220
7.50	161	176	191	206	221
8.50	162	177	192	207	222
9.00	163*	178	193	208	223
9.50	164*	179*	194*	209*	224*

* Values not used

ASYMMETRIC (LEVEL ROLLS)

SWEEP ANGLE PLUS ACCELERATION (1)

$25^\circ + \dot{p}$	$35^\circ + \dot{p}$	$45^\circ + \dot{p}$	$55^\circ + \dot{p}$	$68^\circ + \dot{p}$
226=156+2(92)	231=171+2(99)	237=186+2(104)	243=201+2(110)	249=216+2(114)
226=156-2(92)	232=171-2(99)	238=186-2(104)	244=201-2(110)	250=216-2(114)
227=156+4(92)	233=171+4(99)	239=186+4(104)	245=201+4(110)	251=216+4(114)
228=156-4(92)	234=171-4(99)	240=186-4(104)	246=201-4(110)	252=216-4(114)
229=156+6(92)	235=171+6(99)	241=186+6(104)	247=201+6(110)	253=216+6(114)
230=156-6(92)	236=171-6(99)	242=186-6(104)	248=201-6(110)	254=216-6(114)

1. Example Condition = 1 g + $\dot{p}$ (unit load)

TABLE I Description of Flight and Ground Loading Conditions, Aircraft #98 Fatigue Test (Continued)

CONDITION NUMBERING

ASYMMETRIC (TURN REVERSALS)

SWEEP ANGLE PLUS ACCELERATION

N_z	$25^\circ + \dot{p}$	$35^\circ + \dot{p}$	$45^\circ + \dot{p}$
	255 =157+1.833(93)	280 =172+1.833(100)	305 =187+1.833(105)
	256 =157-1.833(93)	281 =172-1.833(100)	306 =187-1.833(105)
3.5	257 =157+3.500(93)	282 =172-3.500(100)	307 =187-3.500(105)
	258 =157-3.500(93)	283 =172-3.500(100)	308 =187-3.500(105)
	259 =157+5.167(93)	284 =172-5.167(100)	309 =187+5.167(105)
	260 =157-5.167(93)	285 =172-5.167(100)	310 =187-5.167(105)
	261 =158-1.833(93)	286 =173-1.833(100)	311 =188-1.833(105)
	262 =158-1.833(93)	287 =173-1.833(100)	312 =188-1.833(105)
4.5	263 =158+3.500(93)	288 =173+3.500(100)	313 =188+3.500(105)
	264 =158-3.500(93)	289 =173-3.500(100)	314 =188-3.500(105)
	265 =158+5.167(93)	290 =173+5.167(100)	315 =188+5.167(105)
	266 =158-5.167(93)	291 =173-5.167(100)	316 =188-5.167(105)
	267 =159+1.833(93)	292 =174+1.833(100)	317 =189+1.833(105)
	268 =159-1.833(93)	293 =174-1.833(100)	318 =189-1.833(105)
5.5	269 =159+3.500(93)	294 =174+3.500(100)	319 =189+3.500(105)
	270 =159-3.500(93)	295 =174-3.500(100)	320 =189-3.500(105)
	271 =159+5.167(93)	296 =174+5.167(100)	321 =189+5.167(105)
	272 =159-5.167(93)	297 =174-5.167(100)	322 =189-5.167(105)
	273 =160+2.000(93)	298 =175+2.000(100)	323 =190+2.000(105)
6.5	274 =160-2.000(93)	299 =175-2.000(100)	324 =190-2.000(105)
	275 =160+4.000(93)	300 =175+4.000(100)	325 =190+4.000(105)
	276 =160-4.000(93)	301 =175-4.000(100)	326 =190-4.000(105)
	277 =161+2.000(93)	302 =176+2.000(100)	327 =191+2.000(105)
7.5	278 =161-2.000(93)	303 =176-2.000(100)	328 =191-2.000(105)
	279*	304*	329*

*Values not used

TABLE I Description of Flight and Ground Loading Conditions, Aircraft #98 Fatigue Test (Continued)

CONDITION NUMBERING

ASYMMETRIC (TURN REVERSALS) (Cont')

SWEEP ANGLE PLUS ACCELERATION

N_z	$55° + \dot{p}$	$68° + \dot{p}$
	330 =202+1.833(111)	355 =217+1.833(116)
	331 =202-1.833(111)	356 =217-1.833(116)
3.5	332 =202+3.500(111)	357 =217+3.500(116)
	333 =202-3.500(111)	358 =217-3.500(116)
	334 =202+5.167(111)	359 =217+5.167(116)
	335 =202-5.167(111)	360 =217-5.167(116)
	336 =203-1.833(111)	361 =218-1.833(116)
	337 =203-1.833(111)	362 =218-1.833(116)
4.5	338 =203+3.500(111)	363 =218+3.500(116)
	339 =203-3.500(111)	364 =218-3.500(116)
	340 =203+5.167(111)	365 =218+5.167(116)
	341 =203-5.167(111)	366 =218-5.167(116)
	342 =204+1.833(111)	367 =219-1.833(116)
	343 =204-1.833(111)	368 =219-1.833(116)
5.5	344 =204+3.500(111)	369 =219-3.500(116)
	345 =204-3.500(111)	370 =219-3.500(116)
	346 =204+5.167(111)	371 =219+5.167(116)
	347 =204-5.167(111)	372 =219-5.167(116)
	348 =205-2.000(111)	373 =220+2.000(116)
6.5	349 =205-2.000(111)	374 =220-2.000(116)
	350 =205+4.000(111)	375 =220-4.000(116)
	351 =205-4.000(111)	376 =220-4.000(116)
	352 =206-2.000(111)	377 =221-2.000(116)
7.5	353 =206-2.000(111)	378 =221-2.000(116)
	354*	379 MAXIMUM VALUE 1 - 378
		380 MINIMUM VALUE 1 - 378

* VALUE NOT USED

TABLE II Loading Conditions for F 14 Wing Outer Panel Fatigue Test

Condition No.	A/C 93 Test	WOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) H_x	(10^6) $H_{y'}$	Description
1	1	1	0	20112	-1.681	0.862	0	1.857	0.349	Landing 25.3 FPS, tail dn symm
2	1	0								
3	1	0								
4	1	0								
5	3	10	0	16972	1.419	0.728	0	-1.567	-0.295	Landing 23.0 FPS, tail dn symm
6	3	0								
7	3	0								
8	3	0								
9	23	76	0	11177	-0.934	0.479	0	-1.032	0.194	Landing 18.0 FPS, tail dn symm
10	23	0								
11	23	0								
12	23	0								
13	51	174	0	7559	-0.632	0.324	0	-0.698	0.131	Landing 14.0 FPS, tail dn symm
14	51	0								
15	51	0								
16	51	0								
17	56	187	0	-4846	-0.405	0.208	0	-0.448	0.084	Landing 10.0 FPS, tail dn symm
18	56	0								
19	56	0								
20	66	216	0	-3037	0.254	0.130	0	-0.280	0.053	Landing 6.0 FPS, tail dn symm
21	66	0								
22	66	0								
23	0	0	same as condition 1							Landing 25.3 FPS, level
24	0	0								
25	0	0								
26	0	0								
27	3	0	same as condition 5							Landing 23.0 FPS, level
28	3	0								
29	3	0								
30	23	0	same as condition 9							Landing 18.0 FPS, level

TABLE II Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	% of 9.0 g	MOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description
31	53	0								
32	53	0								
33	53	0	Same as condition 13							Landing 14.0 FPS, level
34	53	0								
35	53	0								
36	57	0	Same as condition 17							Landing 10.0 FPS, level
37	57	0								
38	66	0	Same as condition 20							Landing 6.0 FPS, level
39	66	0								
40	0	0	Same as condition 1							Landing 25.3 FPS, tail dn roll rt
41	0	0								
42	0	0								
43	0	0								
44	9	0	Same as condition 5							Landing 23.0 FPS, tail dn roll rt
45	9	0								
46	9	0								
47	9	0								
48	15	0	Same as condition 9							Landing 18.0 FPS, tail dn roll rt
49	15	0								
50	15	0								
51	15	0								
52	35	0	Same as condition 13							Landing 14.0 FPS, tail dn roll rt
53	35	0								
54	35	0								
55	35	0								
56	47	0	Same as condition 17							Landing 10.0 FPS, tail dn roll rt
57	47	0								
58	47	0	Same as condition 20							Landing 6.0 FPS, tail dn roll rt
59	47	0								
60	9	48	6398	184	0.015	0.008	0.535	0.017	-0.093	Arrest, D = 171000, S = 27000, lt

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TABLE II. Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	SAC 96 Test	MOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) M_x'	(10^6) M_y'	Description
61	10	0	same as condition 60							Arrest, D = 171000, S = 16200, lt
62	11	112	5950	171	0.014	0.007	0.497	0.016	-0.003	Arrest, D = 159000, S = 27000, lt
63	55	0	same as condition 62							Arrest, D = 159000, S = 16200, lt
64	2	0	same as condition 60							
65	10	0	same as condition 60							
66	2	0	same as condition 60							Arrest, D = 171000, S = 27000, rt
67	10	0	same as condition 60							Arrest, D = 171000, S = 16200, rt
68	11	0	same as condition 62							Arrest, D = 159000, S = 27000, rt
69	55	0	same as condition 62							Arrest, D = 159000, S = 16200, rt
70	2	0	same as condition 60							
71	10	0	same as condition 60							
72	32	16	14822	-4597	0.418	0.204	-1.349	0.459	0.077	Catapult, T = 237000
73	128	64	13432	-4552	-0.414	0.202	-1.223	-0.455	0.076	Catapult, T = 213000
74	160	80	11521	-4490	-0.409	0.199	-1.049	-0.448	0.075	Catapult, T = 180000
75	32	0								
76	128	0								
77	160	0								
78	32	0								
79	128	0								
80	160	0								
81	160	0								
82	160	0								
83	160	0								
84	320	160	0	-4127	0.376	0.183	0	0.412	0.069	Static ground, 100% fuel
85	361	361	0	-2019	-0.169	0.087	0	-0.186	0.035	Static ground, 30% fuel
86	0	0	0	26418	3.011	1.419	0	3.322	0.217	25^o symm -2.25 g
87	3080	2040	0	43962	5.130	-2.355	0	5.636	-0.311	25^o symm 3.46 g
88	0	0	0	40938	4.575	2.535	0	5.186	-0.682	25^o symm 5.346 g
89	0	0	0	38661	4.075	-2.764	0	4.804	-1.078	25^o symm 6.843 g
90	0	0	0	37442	3.575	3.128	0	4.473	-1.600	25^o symm 7.932 g

TABLE II Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	7.5G 95% Test	BOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description
91	15	15	0	37637	3.250	3.499	0	4.306	-2.065	25° symm 8.243 g
92	0	0	0	975	-0.104	0.059	0	0.118	0.016	25° anti 1.0 g
93	0	0	same as condition 92							25° anti 3.5 g
94	0	0	0	-22162	-2.306	1.629	0	2.817	0.184	35° symm -2.25 g
95	406	253	0	52389	5.351	3.705	0	6.498	-0.363	35° symm 3.75 g
96	52	42	0	50212	4.981	4.018	0	6.346	-0.824	35° symm 6.5 g
97	0	0	0	50110	4.588	-4.441	0	6.232	1.390	35° symm 8.123 g
98	5	4	0	51362	4.385	-4.928	0	6.314	1.911	35° symm 9.0 g
99	0	0	0	923	0.087	0.071	0	-0.111	0.016	35° anti 1.0 g
100	0	0	same as condition 99							35° anti 3.5 g
101	0	0	0	-23116	-2.097	1.958	0	-2.868	0.077	45° symm -2.25 g
102	0	0	0	56752	5.038	-4.831	0	6.974	-0.280	45° symm 4.272 g
103	1	1	0	63550	4.599	-6.136	0	7.510	-1.549	45° symm 9.0 g
104	0	0	0	-860	-0.067	0.079	0	-0.102	0.014	45° anti 1.0 g
105	0	0	same as condition 104							45° anti 3.5 g
106	0	0	0	-17733	-1.338	-1.660	0	-2.132	-0.014	55° symm -2.25 g
107	0	0	0	58901	4.548	-5.529	0	7.158	0.117	55° symm 5.068 g
108	0	0	0	69723	4.744	-7.854	0	9.100	-1.177	55° symm 8.078 g
109	0	0	0	69781	4.624	-8.146	0	9.254	-1.453	55° symm 9.0 g
110	0	0	0	785	0.047	0.080	0	-0.092	0.013	55° anti 1.0 g
111	0	0	same as condition 110							55° anti 3.5 g
112	0	0	0	9070	-0.764	1.139	0	-1.357	-0.199	68° symm -2.253 g
113	0	0	0	58324	4.322	6.980	0	8.161	0.895	68° symm 6.875 g
114	1	1	0	67118	4.608	-8.048	0	9.248	0.694	68° symm 9.0 g
115	0	0	0	685	0.023	0.074	0	-0.077	0.012	68° anti 1.0 g
116	0	0	same as condition 115							68° anti 3.5 g
117	0	0								
118	0	0								
119	0	0								
120	0	0								

TABLE II Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	% of 56 KIP Test	MOP Test	F_x	F_z	M_x (10^6)	M_y (10^6)	M_z (10^6)	$M_{x'}$	$M_{y'}$	Description
121	0	0								
122	0	0								
123	0	0								
124	0	0								
125	0	0								
126	0	0								
127	0	0								
128	0	0								
129	0	0								
130	0	0	Same as condition 1							Landing 25.3 FPS, tail dn roll lt
131	0	0								
132	0	0								
133	0	0								
134	2	0	Same as condition 5							Landing 23.0 FPS, tail dn roll lt
135	2	0								
136	2	0								
137	2	0								
138	15	0	Same as condition 9							Landing 18.0 FPS, tail dn roll lt
139	15	0								
140	15	0								
141	15	0								
142	35	0	Same as condition 13							Landing 14.0 FPS, tail dn roll lt
143	35	0								
144	35	0								
145	35	0								
146	37	0	Same as condition 17							Landing 10.0 FPS, tail dn roll lt
147	37	0								
148	57	0	Same as condition 20							Landing 6.0 FPS, tail dn roll lt
149	57	0								
150	0	0								

TABLE 11 Loading Conditions for F 14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	A/C 98 Test	MOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description
151	3	3	0	14092	1.586	0.759	0	-1.754	0.125	25° symm -1.25 g
152	9	9	0	7933	-0.869	0.429	0	-0.966	0.081	25° symm -0.75 g
153	42	42	0	1769	-0.157	0.099	0	-0.182	0.035	25° symm -0.25 g
154	314	314	0	4395	0.055	-0.232	0	0.136	-0.196	25° symm 0.25 g
155	2752	2752	0	10559	1.267	-0.562	0	1.385	-0.059	25° symm 0.75 g
156	8438	3502	0	13641	1.623	-0.729	0	1.777	-0.083	25° symm 1.00 g
157	1722	1722	0	43898	5.118	-2.358	0	5.626	-0.318	25° symm 3.50 g
158	812	812	0	42295	4.824	-2.453	0	5.387	-0.514	25° symm 4.50 g
159	371	371	0	40703	4.524	-2.559	0	5.147	-0.723	25° symm 5.50 g
160	143	143	0	39182	4.190	-2.712	0	4.892	-0.988	25° symm 6.50 g
161	57	57	0	37926	3.773	-2.982	0	4.603	-1.392	25° symm 7.50 g
162	0	0	0	37798	2.981	-3.806	0	4.168	-2.449	25° symm 8.50 g
163	0	0								
164	0	0								
165	0	0								
166	0	0								
167	2	2	0	-3523	-0.392	0.296	0	-0.489	0.048	35° symm -0.75 g
168	13	13	0	2690	0.246	-0.149	0	0.288	0.001	35° symm -0.25 g
169	93	93	0	8903	0.884	-0.594	0	1.064	-0.045	35° symm 0.25 g
170	816	816	0	15116	1.522	-1.039	0	1.841	-0.091	35° symm 0.75 g
171	2100	844	0	18220	1.842	-1.260	0	2.229	-0.112	35° symm 1.00 g
172	507	507	0	49282	5.032	-3.483	0	6.110	-0.341	35° symm 3.50 g
173	240	240	0	51795	5.250	-3.790	0	6.457	-0.489	35° symm 4.50 g
174	110	110	0	51004	5.116	-3.904	0	6.402	-0.656	35° symm 5.50 g
175	0	0	0	50212	4.981	-4.018	0	6.346	-0.824	35° symm 6.50 g
176	17	17	0	50149	4.739	-4.279	0	6.276	-1.173	35° symm 7.50 g
177	4	4	0	50648	4.439	-4.650	0	6.214	-1.646	35° symm 8.50 g
178	0	0	0	51362	4.385	-4.928	0	6.314	-1.911	35° symm 9.0 g
179	0	0								

TABLE II Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	A/C 98 Test	MOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description	
181	0	0									
182	0	0									
183	9	9	0	1375	0.091	0.124	0	0.150	-0.033	45° symm	-0.25 g
184	64	64	0	7498	0.638	-0.645	0	0.905	-0.060	45° symm	0.25 g
185	557	557	0	13621	1.185	-1.166	0	1.660	-0.088	45° symm	0.75 g
186	1422	577	0	16683	1.458	-1.425	0	2.036	-0.101	45° symm	1.00 g
187	345	345	0	47298	4.193	-4.027	0	5.809	-0.238	45° symm	3.50 g
188	165	165	0	57080	5.017	-4.894	0	7.000	-0.341	45° symm	4.50 g
189	75	75	0	58518	4.924	-5.170	0	7.114	-0.610	45° symm	5.50 g
190	29	29	0	59955	4.831	-5.446	0	7.227	-0.878	45° symm	6.50 g
191	12	12	0	61393	4.738	-5.722	0	7.340	-0.146	45° symm	7.50 g
192	3	3	0	62831	4.645	-5.998	0	7.453	-0.415	45° symm	8.50 g
193	0	0	0	63550	4.599	-6.136	0	7.510	-1.549	45° symm	9.0 g
194	0	0									
195	0	0									
196	0	0									
197	0	0									
198	7	7	0	3210	0.270	-0.305	0	0.407	0.021	55° symm	-0.25 g
199	41	41	0	8447	0.672	-0.796	0	1.041	0.030	55° symm	0.25 g
200	360	360	0	13684	1.074	-1.287	0	1.676	0.039	55° symm	0.75 g
201	936	373	0	16300	1.276	-1.533	0	1.994	0.044	55° symm	1.0 g
202	228	228	0	42480	3.286	-3.989	0	5.167	0.088	55° symm	3.50 g
203	105	105	0	52952	4.091	-4.971	0	6.437	0.107	55° symm	4.50 g
204	48	48	0	60454	4.576	-5.863	0	7.437	-0.069	55° symm	5.50 g
205	18	18	0	64050	4.641	-6.635	0	8.082	-0.499	55° symm	6.50 g
206	7	7	0	67645	4.706	-7.408	0	8.727	-0.929	55° symm	7.50 g
207	2	2	0	69750	4.689	-7.988	0	9.170	-1.304	55° symm	8.50 g
208	0	0	0	69781	4.624	-8.146	0	9.254	-1.453	55° symm	9.0 g
209	0	0									
210	0	0									

TABLE II Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	S/C 98 Test	MOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description
211	0	0								
212	4	4	0	20638	0.073	-0.198	0	0.210	-0.019	68^o symm -0.75 g
213	9	9	0	5757	.353	-0.643	0	0.732	0.041	68^o symm -0.25 g
214	69	69	0	9446	.631	-1.088	0	1.254	0.101	68^o symm 0.25 g
215	600	600	0	13135	.909	-1.533	0	1.775	0.160	68^o symm 0.75 g
216	1518	613	0	14980	1.049	-1.754	0	2.035	0.192	68^o symm 1.0 g
217	371	371	0	33424	2.441	-3.978	0	4.641	0.490	68^o symm 3.50 g
218	181	181	0	40802	2.999	-4.868	0	5.685	0.611	68^o symm 4.50 g
219	83	83	0	48180	3.556	-5.757	0	6.727	0.731	68^o symm 5.50 g
220	31	31	0	55557	4.113	-6.646	0	7.769	0.851	68^o symm 6.50 g
221	12	12	0	60910	4.406	-7.294	0	8.480	0.836	68^o symm 7.50 g
222	3	3	0	65049	4.541	-7.794	0	8.990	0.743	68^o symm 8.50 g
223	0	0	0	67118	4.608	-8.048	0	9.248	0.694	68^o symm 9.0 g
224	0	0								
225	0	0	0	15591	1.415	-0.611	0	1.540	-0.050	25^o level roll 2 rad/sec^2
226	0	0	0	11691	1.831	-0.847	0	2.014	-0.117	25^o level roll -2 rad/sec^2
227	376	376	0	17541	1.207	-0.493	0	1.304	-0.016	25^o level roll 4 rad/sec^2
228	376	376	0	9741	2.039	-0.965	0	2.251	-0.151	25^o level roll -4 rad/sec^2
229	143	143	0	19491	0.999	-0.375	0	1.067	0.017	25^o level roll 6 rad/sec^2
230	143	143	0	7791	2.247	-1.083	0	2.488	-0.184	25^o level roll -6 rad/sec^2
231	0	0	0	20066	1.668	-1.118	0	2.006	-0.082	35^o level roll 2 rad/sec^2
232	0	0	0	16374	2.016	-1.402	0	2.451	-0.142	35^o level roll -2 rad/sec^2
233	111	111	0	21912	1.494	-0.976	0	1.784	-0.052	35^o level roll 4 rad/sec^2
234	111	111	0	14528	2.190	-1.544	0	2.674	-0.172	35^o level roll -4 rad/sec^2
235	42	42	0	23758	1.320	-0.834	0	1.561	-0.021	35^o level roll 6 rad/sec^2
236	42	42	0	12687	2.364	-1.686	0	2.897	-0.202	35^o level roll -6 rad/sec^2
237	0	0	0	18403	1.324	-1.267	0	1.831	-0.072	45^o level roll 2 rad/sec^2
238	0	0	0	14963	1.592	-1.583	0	2.241	-0.131	45^o level roll -2 rad/sec^2
239	77	77	0	20123	1.190	-1.109	0	1.626	-0.042	45^o level roll 4 rad/sec^2
240	77	77	0	13243	1.726	-1.741	0	2.446	-0.160	45^o level roll -4 rad/sec^2

TABLE II Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	Cycles	MOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description
234	29	29	0	21843	1.056	-0.951	0	1.421	0.013	45° level roll 6 rad/sec^2
235	29	29	0	11523	1.860	-1.899	0	2.651	-0.190	45° level roll -6 rad/sec^2
236	0	0	0	17876	1.182	-1.373	0	1.810	0.070	55° level roll 2 rad/sec^2
237	0	0	0	14724	1.370	-1.693	0	2.178	0.018	55° level roll -2 rad/sec^2
238	48	48	0	19452	1.088	-1.213	0	1.627	0.096	55° level roll 4 rad/sec^2
239	48	48	0	13148	1.464	-1.853	0	2.362	-0.008	55° level roll -4 rad/sec^2
240	18	18	0	21028	0.994	-1.053	0	1.443	0.122	55° level roll 6 rad/sec^2
241	18	18	0	11572	1.558	-2.013	0	2.545	-0.034	55° level roll -6 rad/sec^2
242	0	0	0	16350	1.003	-1.606	0	1.881	0.214	68° level roll 2 rad/sec^2
243	0	0	0	13610	1.095	-1.902	0	2.188	0.169	68° level roll -2 rad/sec^2
244	84	84	0	17720	0.957	-1.458	0	1.728	0.236	68° level roll 4 rad/sec^2
245	84	84	0	12240	1.141	-2.05	0	2.342	0.147	68° level roll -4 rad/sec^2
246	32	32	0	19090	0.911	-1.310	0	1.575	0.258	68° level roll 6 rad/sec^2
247	32	32	0	10870	1.187	-2.198	0	2.495	0.125	68° level roll -6 rad/sec^2
248	464	464	0	45685	4.927	-2.250	0	5.409	-0.288	25° turn, 3.5 g & 1.833
249	464	464	0	42111	5.309	-2.466	0	5.843	-0.349	25° turn, 3.5 g & -1.833
250	47	47	0	47311	4.754	-2.152	0	5.212	-0.260	25° turn, 3.5 g & 3.500
251	47	47	0	40486	5.482	-2.565	0	6.040	-0.377	25° turn, 3.5 g & -3.500
252	11	11	0	48936	4.581	-2.053	0	5.014	-0.232	25° turn, 3.5 g & 5.167
253	11	11	0	38860	5.655	-2.663	0	6.238	-0.405	25° turn, 3.5 g & -5.167
254	317	317	0	44082	4.633	-2.345	0	5.170	-0.484	25° turn, 4.5 g & 1.833
255	317	317	0	40508	5.015	-2.561	0	5.604	-0.545	25° turn, 4.5 g & -1.833
256	37	37	0	45708	4.460	-2.247	0	4.973	-0.456	25° turn, 4.5 g & 3.500
257	37	37	0	38883	5.188	-2.660	0	5.802	-0.573	25° turn, 4.5 g & -3.500
258	9	9	0	47333	4.287	-2.148	0	4.776	-0.428	25° turn, 4.5 g & 5.167
259	9	9	0	37257	5.361	-2.758	0	5.999	-0.601	25° turn, 4.5 g & -5.167
260	123	123	0	42490	4.333	-2.451	0	4.930	-0.692	25° turn, 5.5 g & 1.833
261	123	123	0	38916	4.715	-2.667	0	5.364	-0.754	25° turn, 5.5 g & -1.833
262	16	16	0	44116	4.160	-2.353	0	4.733	-0.664	25° turn, 5.5 g & 3.500
270	16	16	0	37291	4.888	-2.766	0	5.561	-0.782	25° turn, 5.5 g & -3.500

TABLE II. Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	% of 96 Test	MOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description
271	4	4	0	45741	3.987	-2.254	0	4.595	-0.636	25° turn, 5.5 g & 5.167
272	4	4	0	35665	5.061	-2.864	0	5.759	-0.810	25° turn, 5.5 g & -5.167
273	36	36	0	41137	3.982	-2.594	0	4.656	-0.954	25° turn, 6.5 g & 2.000
274	36	36	0	37232	4.398	-2.830	0	5.129	-1.021	25° turn, 6.5 g & -2.000
275	6	6	0	43082	3.774	-2.476	0	4.419	-0.921	25° turn, 6.5 g & 4.000
276	6	6	0	35282	4.606	-2.948	0	5.366	-1.055	25° turn, 6.5 g & -4.000
277	10	10	0	39876	3.565	-2.864	0	4.367	-1.358	25° turn, 7.5 g & 2.000
278	10	10	0	35976	3.981	-3.100	0	4.840	-1.425	25° turn, 7.5 g & -2.000
279	0	0								
280	127	127	0	50974	4.873	3.353	0	5.906	0.313	35° turn, 3.5 g & 1.833
281	127	127	0	47590	5.191	-3.613	0	6.314	-0.368	35° turn, 3.5 g & -1.833
282	14	14	0	52513	4.728	-3.235	0	5.721	-0.288	35° turn, 3.5 g & 3.500
283	14	14	0	46052	5.337	-3.732	0	6.500	-0.394	35° turn, 3.5 g & -3.500
284	3	3	0	54051	4.582	-3.116	0	5.535	-0.263	35° turn, 3.5 g & 5.167
285	3	3	0	44513	5.482	-3.850	0	6.685	-0.419	35° turn, 3.5 g & -5.167
286	94	94	0	53487	5.091	-3.660	0	6.253	-0.461	35° turn, 4.5 g & 1.833
287	94	94	0	50103	5.409	-3.920	0	6.661	-0.516	35° turn, 4.5 g & -1.833
288	11	11	0	55026	4.946	-3.542	0	6.067	-0.436	35° turn, 4.5 g & 3.500
289	11	11	0	48565	5.555	-4.039	0	6.846	-0.541	35° turn, 4.5 g & -3.500
290	2	2	0	56564	4.800	-3.423	0	5.882	-0.411	35° turn, 4.5 g & 5.167
291	2	2	0	47026	5.700	4.157	0	7.032	-0.567	35° turn, 4.5 g & -5.167
292	36	36	0	52696	4.957	-3.774	0	6.198	-0.628	35° turn, 5.5 g & 1.833
293	36	36	0	49317	5.275	-4.034	0	6.606	-0.683	35° turn, 5.5 g & -1.833
294	5	5	0	54235	4.812	-3.656	0	6.012	-0.603	35° turn, 5.5 g & 3.500
295	5	5	0	47774	5.421	-4.153	0	6.791	-0.709	35° turn, 5.5 g & -3.500
296	1	1	0	55773	4.666	-3.537	0	5.827	-0.578	35° turn, 5.5 g & 5.167
297	1	1	0	46235	5.566	-4.271	0	6.977	-0.734	35° turn, 5.5 g & -5.167
298	10	10	0	52058	4.807	-3.876	0	6.124	-0.793	35° turn, 6.5 g & 2.000
299	10	10	0	48366	5.155	-4.160	0	6.569	-0.854	35° turn, 6.5 g & -2.000
300	2	2	0	53904	4.633	-3.734	0	5.901	-0.763	35° turn, 6.5 g & 4.000

TABLE II Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	VFC-96 Test	MOP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description
301	2	2	0	46520	5.329	-4.302	0	6.791	-0.884	35^o turn, 6.5 g & 4.000
302	3	3	0	51995	4.565	-4.137	0	6.054	-1.142	35^o turn, 7.5 g & 2.000
303	3	3	0	48303	4.913	-4.421	0	6.499	-1.203	35^o turn, 7.5 g & -2.000
304	0	0								
305	91	91	0	48874	4.070	3.882	0	5.621	-0.211	45^o turn, 3.5 g & 1.833
306	91	91	0	45722	4.316	-4.172	0	5.997	-0.265	45^o turn, 3.5 g & -1.833
307	9	9	0	50308	3.959	-3.751	0	5.450	-0.186	45^o turn, 3.5 g & 3.500
308	9	9	0	44288	4.428	-4.304	0	6.168	-0.290	45^o turn, 3.5 g & -3.500
309	2	2	0	51742	3.847	-3.619	0	5.279	-0.162	45^o turn, 3.5 g & 5.167
310	2	2	0	42854	4.539	-4.435	0	6.338	-0.314	45^o turn, 3.5 g & -5.167
311	64	64	0	58656	4.894	-4.749	0	6.812	-0.314	45^o turn, 4.5 g & 1.833
312	64	64	0	55504	5.140	-5.039	0	7.188	-0.368	45^o turn, 4.5 g & -1.833
313	8	8	0	60090	4.783	-4.618	0	6.642	-0.290	45^o turn, 4.5 g & 3.500
314	8	8	0	54070	5.252	-5.171	0	7.359	-0.393	45^o turn, 4.5 g & -3.500
315	2	2	0	61524	4.671	-4.486	0	6.471	-0.265	45^o turn, 4.5 g & 5.167
316	2	2	0	52636	5.363	-5.302	0	7.530	-0.418	45^o turn, 4.5 g & -5.16
317	25	25	0	60094	4.801	-5.025	0	6.926	-0.583	45^o turn, 5.5 g & 1.833
318	25	25	0	56942	5.047	-5.315	0	7.302	-0.637	45^o turn, 5.5 g & -1.833
319	3	3	0	61528	4.690	-4.894	0	6.755	-0.558	45^o turn, 5.5 g & 3.500
320	3	3	0	55508	5.159	-5.447	0	7.472	-0.661	45^o turn, 5.5 g & -3.500
321	1	1	0	62962	4.578	-4.762	0	6.584	-0.533	45^o turn, 5.5 g & 5.167
322	1	1	0	54074	5.270	-5.578	0	7.643	-0.686	45^o turn, 5.5 g & -5.167
323	8	8	0	61675	4.697	-5.288	0	7.022	-0.849	45^o turn, 6.5 g & 2.000
324	8	8	0	58235	4.965	-5.604	0	7.432	-0.908	45^o turn, 6.5 g & -2.000
325	1	1	0	63395	4.563	-5.130	0	6.817	-0.819	45^o turn, 6.5 g & 4.000
326	1	1	0	56515	5.099	-5.762	0	7.637	-0.937	45^o turn, 6.5 g & -4.000
327	2	2	0	63113	4.604	-5.564	0	7.135	-1.117	45^o turn, 7.5 g & 2.000
328	2	2	0	59673	4.872	-5.880	0	7.545	-1.176	45^o turn, 7.5 g & -2.000
329	0	0								
330	60	60	0	44924	3.200	-3.842	0	4.999	-0.112	55^o turn, 3.5 g & 1.833

TABLE II. Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	% Of 95 Test	WoP Test	F_x	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description
331	60	60	0	41036	3.372	-4.136	0	5.336	0.064	55^o turn, 3.5 g & -1.833
332	6	6	0	45238	3.122	-3.709	0	4.856	0.134	55^o turn, 3.5 g & 3.500
333	6	6	0	39722	3.451	-4.269	0	5.489	0.043	55^o turn, 3.5 g & -3.500
334	1	1	0	46552	3.043	-3.576	0	4.693	0.155	55^o turn, 3.5 g & 5.167
335	1	1	0	38408	3.529	-4.402	0	5.642	0.021	55^o turn, 3.5 g & -5.167
336	41	41	0	54396	4.005	-4.824	0	6.269	0.131	55^o turn, 4.5 g & 1.833
337	41	41	0	51508	4.177	-5.118	0	6.605	0.083	55^o turn, 4.5 g & -1.833
338	5	5	0	55710	3.927	-4.691	0	6.116	0.152	55^o turn, 4.5 g & 3.500
339	5	5	0	50194	4.256	-5.251	0	6.759	0.061	55^o turn, 4.5 g & -3.500
340	1	1	0	57024	3.848	-4.558	0	5.962	0.174	55^o turn, 4.5 g & 5.167
341	1	1	0	48880	4.334	-5.384	0	6.912	0.039	55^o turn, 4.5 g & -5.167
342	16	16	0	61898	4.490	-5.716	0	7.269	-0.045	55^o turn, 5.5 g & 1.833
343	16	16	0	59010	4.662	-6.010	0	7.605	-0.093	55^o turn, 5.5 g & -1.833
344	2	2	0	63212	4.412	-5.583	0	7.116	-0.023	55^o turn, 5.5 g & 3.500
345	2	2	0	57696	4.741	-6.143	0	7.759	-0.115	55^o turn, 5.5 g & -3.500
346	0	0	0	64526	4.333	-5.450	0	6.967	-0.002	55^o turn, 5.5 g & 5.167
347	0	0	0	56382	4.819	-6.276	0	7.912	-0.136	55^o turn, 5.5 g & -5.167
348	4	4	0	65626	4.547	-6.475	0	7.898	-0.473	55^o turn, 6.5 g & 2.000
349	4	4	0	62474	4.735	-6.795	0	8.265	-0.525	55^o turn, 6.5 g & -2.000
350	1	1	0	67202	4.453	-6.315	0	7.714	-0.447	55^o turn, 6.5 g & 4.000
351	1	1	0	60898	4.829	-6.955	0	8.449	-0.551	55^o turn, 6.5 g & -4.000
352	1	1	0	69221	4.612	-7.248	0	8.543	-0.903	55^o turn, 7.5 g & 2.000
353	1	1	0	66069	4.800	-7.568	0	8.911	-0.955	55^o turn, 7.5 g & -2.000
354	0	0								
355	95	95	0	34680	2.399	-3.842	0	4.501	0.511	68^o turn, 3.5 g & 1.833
356	95	95	0	32168	2.483	-4.114	0	4.782	0.470	68^o turn, 2.5 g & -1.833
357	10	10	0	35822	2.361	-3.719	0	4.373	0.529	68^o turn, 3.5 g & 3.500
358	10	10	0	31027	2.522	-4.237	0	4.910	0.451	68^o turn, 3.5 g & -3.500
359	2	2	0	36963	2.322	-3.596	0	4.245	0.548	68^o turn, 3.5 g & 5.167
360	2	2	0	29885	2.560	-4.360	0	5.038	0.433	68^o turn, 3.5 g & -5.167

TABLE II. Loading Conditions for F-14 Wing Outer Panel Fatigue Test (Continued)

Condition No.	% of Total	MOP Test	F	F_z	(10^6) M_x	(10^6) M_y	(10^6) M_z	(10^6) $M_{x'}$	(10^6) $M_{y'}$	Description
364	71	71	0	42057	2.957	4.732	0	5.544	0.631	68° turn, 4.5 g & 1.833
365	71	71	0	39546	3.041	5.004	0	5.826	0.590	68° turn, 4.5 g & -1.833
366	8	8	0	43200	2.919	-4.609	0	5.417	0.650	68° turn, 4.5 g & 3.500
367	8	8	0	38405	3.080	-5.127	0	5.953	0.572	68° turn, 4.5 g & -3.500
368	2	2	0	44341	2.880	4.486	0	5.289	0.668	68° turn, 4.5 g & 5.167
369	2	2	0	37263	3.118	-5.250	0	6.081	0.553	68° turn, 4.5 g & -5.167
370	28	28	0	49436	3.514	-5.621	0	6.587	0.751	68° turn, 5.5 g & 1.833
371	28	28	0	46924	3.598	-5.893	0	6.868	0.710	68° turn, 5.5 g & -1.833
372	3	3	0	50578	3.476	5.498	0	6.459	0.769	68° turn, 5.5 g & 3.500
373	3	3	0	45783	3.637	-6.016	0	6.996	0.692	68° turn, 5.5 g & -3.500
374	1	1	0	51719	3.437	-5.375	0	6.331	0.788	68° turn, 5.5 g & 5.167
375	1	1	0	44641	3.675	-6.139	0	7.123	0.673	68° turn, 5.5 g & -5.167
376	8	8	0	56927	4.067	-6.498	0	7.616	0.873	68° turn, 6.5 g & 2.000
377	8	8	0	54187	4.159	-6.794	0	7.923	0.828	68° turn, 6.5 g & -2.000
378	1	1	0	58297	4.021	-6.350	0	7.463	0.895	68° turn, 6.5 g & 4.000
379	1	1	0	52817	4.205	-6.942	0	8.076	0.806	68° turn, 6.5 g & -4.000
380	2	2	0	62280	4.360	-7.146	0	8.327	0.858	68° turn, 7.5 g & 2.000
381	2	2	0	59540	4.452	-7.442	0	8.634	0.814	68° turn, 7.5 g & -2.000

TABLE III Calculation of Net Wing Pivot Loads for Symmetric Flight Conditions

Condition	Λ	N_z	α	q	F_z/q	M_x/q	M_y/q	$F_{z_{AIR}}$	$M_{x_{AIR}}$ x 10^6	$M_{y_{AIR}}$ x 10^6	F_{z_I}	M_{x_I} x 10^6	M_{y_I} x 10^6	F_z	M_x x 10^6	M_y x 10^6	$M_{x'}$ x 10^6	$M_{y'}$ x 10^6
[illegible]	[illegible]	[illegible]	7.15	391.91	79	8600	4200	-30961	-3.370	-1.646	4543	0.359	-0.227	-26418	-3.011	1.419	-3.321	0.217
87	[illegible]	[illegible]	8.20	391.91	130	[illegible]	6900	50948	5.683	-2.704	-6986	-0.553	0.349	43962	5.130	-2.355	5.636	-0.311
[illegible]	[illegible]	[illegible]	16.0	391.91	132	[illegible]	-7844	51732	5.429	-3.074	-10794	0.854	0.539	40938	4.575	-2.535	5.186	-0.682
89	[illegible]	[illegible]	24.0	391.91	133.9	13187	-8812	52477	5.168	-3.454	-13816	-1.093	0.690	38661	4.075	-2.764	4.804	-1.078
[illegible]	[illegible]	[illegible]	34.0	391.91	136.4	[illegible]	10022	53457	4.842	-3.928	-16015	1.267	0.800	37442	3.575	-3.128	4.473	-1.60
91	[illegible]	[illegible]	42.5	391.91	138.5	[illegible]	11050	54280	4.566	-4.331	-16643	1.316	0.832	37637	3.250	-3.499	4.306	-2.064
[illegible]	[illegible]	[illegible]	6.3	503.864	53	5200	3800	-26705	-2.620	1.915	4543	0.314	-0.286	-22162	-2.306	1.629	-2.820	0.184
[illegible]	[illegible]	[illegible]	7.6	503.864	119	[illegible]	8300	59960	5.895	-4.182	-7571	0.524	0.477	52389	5.351	-3.705	6.50	-0.363
[illegible]	[illegible]	[illegible]	16.0	503.864	125.7	[illegible]	9613	63336	5.807	-4.844	-13124	-0.909	0.826	50212	4.981	-4.018	6.350	-0.824
97	[illegible]	[illegible]	24.0	503.864	132	11358	10863	66510	5.723	-5.473	-16400	1.135	1.032	50110	4.588	-4.441	6.232	-1.390
98	[illegible]	9.0	31.6	503.864	138	11200	-12050	69533	5.643	-6.072	-18171	-1.258	1.144	51362	4.385	-4.928	6.314	-1.911
101	[illegible]	[illegible]	5.7	628.624	44	3750	3650	-27659	2.357	2.294	4543	0.260	-0.336	-23116	-2.097	1.958	-2.868	0.077
102	[illegible]	[illegible]	7.8	628.624	104	8800	8700	65377	5.532	-5.469	-8625	-0.494	0.638	56752	5.038	-4.831	6.974	-0.280
103	[illegible]	9.0	17.5	628.624	130	8570	-11900	81721	5.639	7.481	-18171	-0.040	1.345	63550	4.599	-6.136	7.510	-1.549
106	[illegible]	[illegible]	5.2	768.143	29	2000	2650	-22276	-1.536	2.036	4543	0.198	-0.376	-17733	-1.338	1.660	-2.132	-0.014
107	[illegible]	[illegible]	8.2	768.143	90	6500	-8300	69133	4.993	-6.376	-10232	-.445	0.847	58901	4.548	-5.529	7.158	0.117
108	[illegible]	[illegible]	14.0	768.143	112	7100	-10400	86032	5.454	-7.989	-16309	-0.710	0.135	69723	4.744	-7.854	9.10	-1.177
109	[illegible]	9.0	15.75	768.143	114.5	7050	-10800	87952	5.415	-8.296	-18171	-0.791	0.150	69781	4.624	-8.146	9.253	-1.453
112	[illegible]	[illegible]	3.4	969.196	14	-900	1600	-13569	-0.872	1.551	4549	0.108	-0.412	-9020	-0.764	1.139	-1.357	-0.199
113	[illegible]	[illegible]	10.0	969.196	74.5	4800	-8500	72205	4.652	-8.238	-13831	0.330	1.256	58324	4.322	-6.980	8.161	0.895
114	[illegible]	9.0	13.1	969.196	88	5200	-10000	85289	5.040	-9.692	-18171	0.432	1.644	67118	4.608	-8.048	9.248	0.694

TABLE IV VARIATION OF WING CENTER OF PRESSURE LOCATION WITH SWEEP ANGLE

Wing Sweep Angle, Degrees	[illegible] Inches	[illegible] Inches
25°	122.5	2.1
35°	121.0	2.1
45°	120.0	0.0
55°	115.9	-4.0
65°	110.0	-10.1

TABLE V SUMMARY OF C.G. LOAD FACTORS FOR ARRESTED LANDING CONDITIONS: AIRCRAFT NO. 98 FATIGUE TEST

Condition No.	Description	Drag, lb	N_x	N_z
60, 61, 66, 67 64, 65, 70, 71	Upper 90%	171000	3.169	-.0913
62, 63, 68, 69	Mean	159000	2.947	-.0849

Notes: - Taken from reference (c)
- N_y and angular accelerations omitted
- 148,000 lb conditions (64, 65, 70, 71) combined with 171,000 lb conditions per NAVAIR direction

TABLE VI SUMMARY OF C.G. LOAD FACTORS FOR CATAPULT CONDITIONS: AIRCRAFT NO. 98 FATIGUE TEST

Condition No.	Description	N_x	N_z
72	Tow = 237000 lb	3.592	1.114
73	Tow = 213000 lb	3.055	1.103
74	Tow = 180000 lb	2.792	1.088

Notes: Taken from reference (c)
- N_y and angular accelerations zero

TABLE VII - SUMMARY OF EVENTS INCLUDED IN F-14 VTXO OUTER PANEL FATIGUE TEST SPECTRUM

BASED ON A BLOCK SIZE OF 440 FLIGHTS (480 HOURS)

FLIGHT

MANEUVERS VERSUS WING SWEEP

	1	2	3	4	5	6
Sweep	Symmetric	Turn Reversals	Level Rolls	Asymmetric 2 + 3	Maneuvers at $N_z > 1.0$ $1^z + 2$	Total Maneuvers 1 + 4
25	2040	1080	519	1599	3120	3639
35	616	308	153	461	924	1077
45	414	216	106	322	630	736
55	270	138	66	204	408	474
68	451	231	116	347	682	798
Sum	3791	1973	960	2933	5764	6724

LANDINGS

SINK SPEED VERSUS CYCLES

Sink Speed	Cycles
25.3	1
23.0	10
18.0	76
14.0	174
10.0	187
6.0	216
Sum	664

CATAPULTS

LAUNCH (TOW) LOAD VERSUS CYCLES

Load	Cycles
237000	16
213000	64
180000	80
Sum	160

ARRESTMENTS

ARRESTMENT LOAD (DRAG) VERSUS CYCLES

Load	Cycles
171000	48
159000	112
Sum	160

CHANGE IN WING SWEEP AT VARIOUS LEVELS OF WING BEARING AXIAL LD CYCLES FOR 185.2 HOURS

BEARING LOAD RANGE < LD ≤		WING SWEEP CHANGE											
		≤ 0.3	< ≤ 2.0	< ≤ 5.0	< ≤ 10.0	< ≤ 15.0	< ≤ 20.0	< ≤ 25.0	< ≤ 30.0	< ≤ 35.0	< ≤ 40.0	< ≤ 45.0	< ≤ 50.0
0.	50000.	57	26	8	2	~	~	~	~	1	~	13	98
50000.	100000.	500	112	92	10	5	1	4	2	~	1	1	~
100000.	150000.	3261	703	411	105	56	35	13	19	22	16	16	~
150000.	200000.	2869	401	169	46	19	14	7	1	~	1	3	~
200000.	250000.	1065	195	69	23	9	9	2	3	4	~	~	~
250000.	300000.	765	160	53	11	3	5	~	1	~	~	~	~
300000.	350000.	741	156	39	7	1	~	~	~	~	~	~	~
350000.	400000.	652	191	58	5	2	~	2	~	~	~	~	~
400000.	450000.	603	193	54	10	2	1	~	~	~	~	~	~
450000.	500000.	435	182	36	1	~	~	~	~	~	~	~	~
500000.	550000.	298	125	25	1	1	~	~	~	~	~	~	~
550000.	600000.	92	27	3	~	~	~	~	~	~	~	~	~
600000.	650000.	20	9	1	~	~	~	~	~	~	~	~	~
650000.	700000.	2	1	~	~	~	~	~	~	~	~	~	~
700000.	750000.	~	~	~	~	~	~	~	~	~	~	~	~
750000.	800000.	~	~	~	~	~	~	~	~	~	~	~	~
800000.	850000.	~	~	~	~	~	~	~	~	~	~	~	~
850000.	900000.	~	~	~	~	~	~	~	~	~	~	~	~

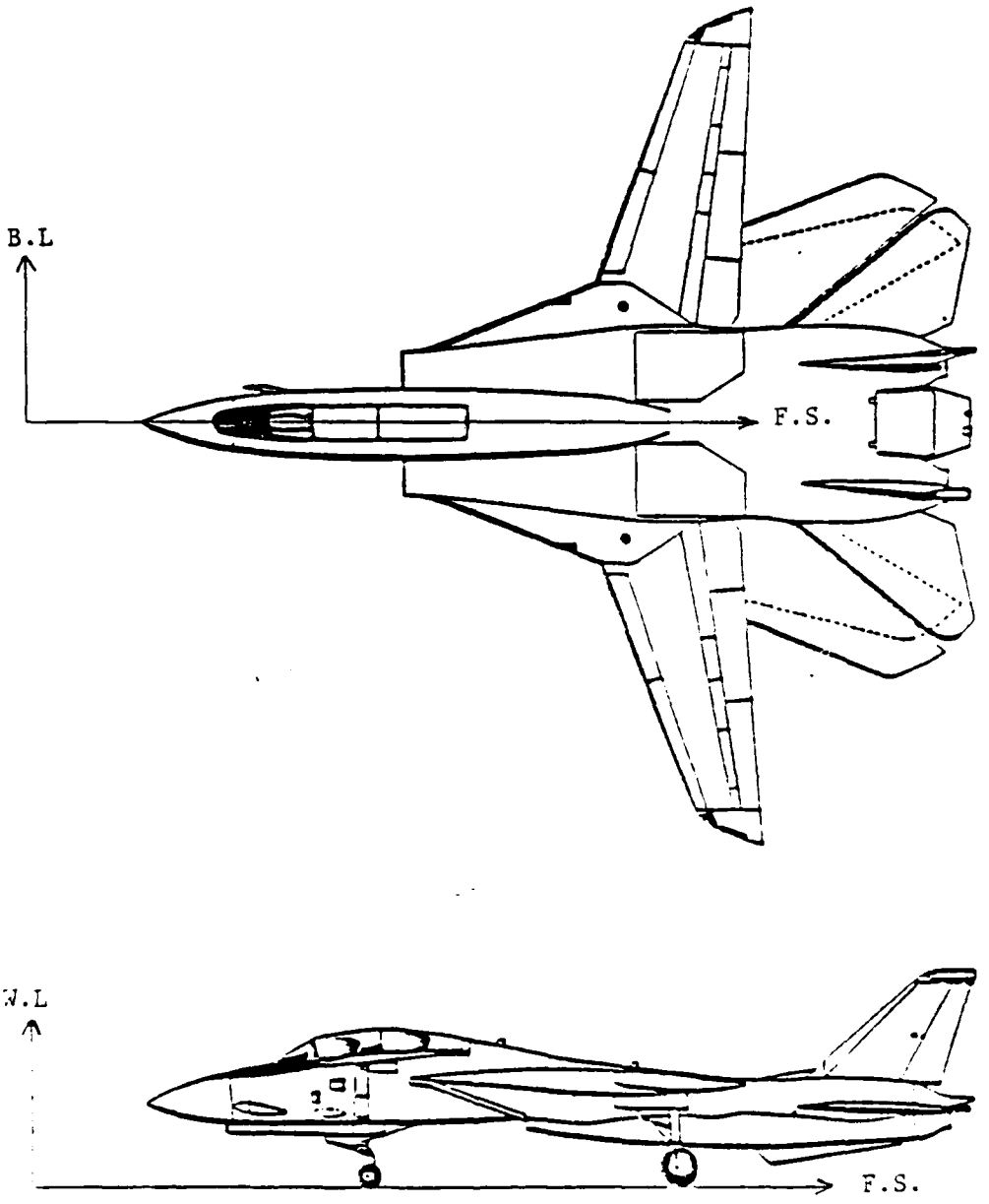
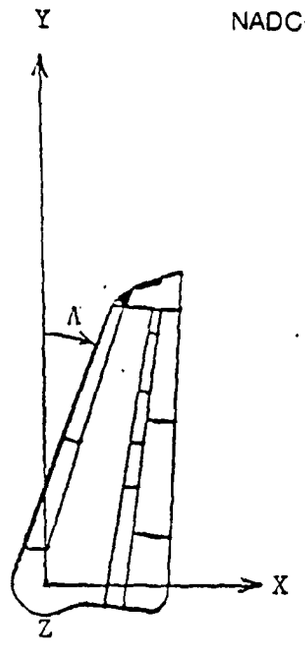


Figure 1. Axes and Sign Conventions

a. Aircraft Axis System

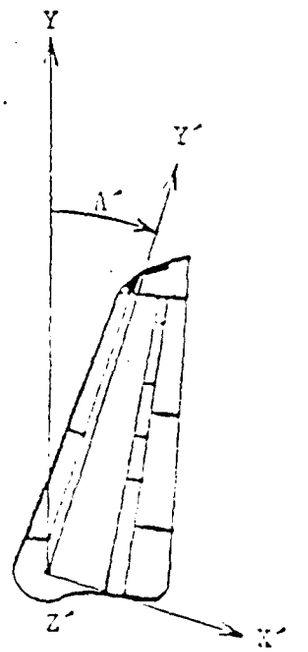


Origin at Wing Pivot Axis

F.S. = 524.203
B.L. = 107.000
W.L. = 145.000

Forces positive as shown
Right hand rule for moments

b. Unswept Wing Axis System



$\Lambda' = \Lambda - 3.5°$

c. Wing Outer Panel Axis System

Figure 1. Axes and Sign Conventions (Cont.)

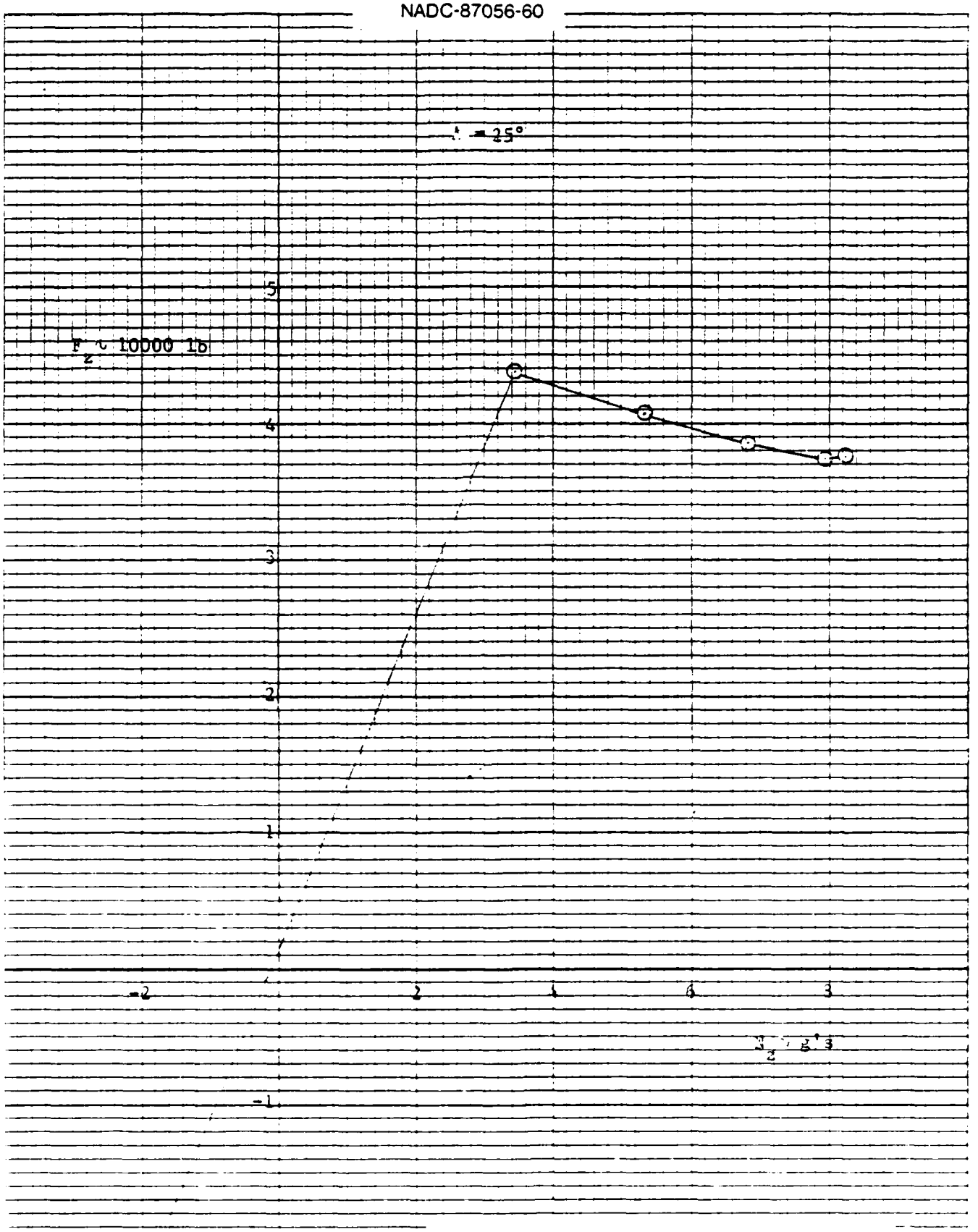


Figure 3. Net Wing Pivot Loads at 25° Sweep

a. Shear

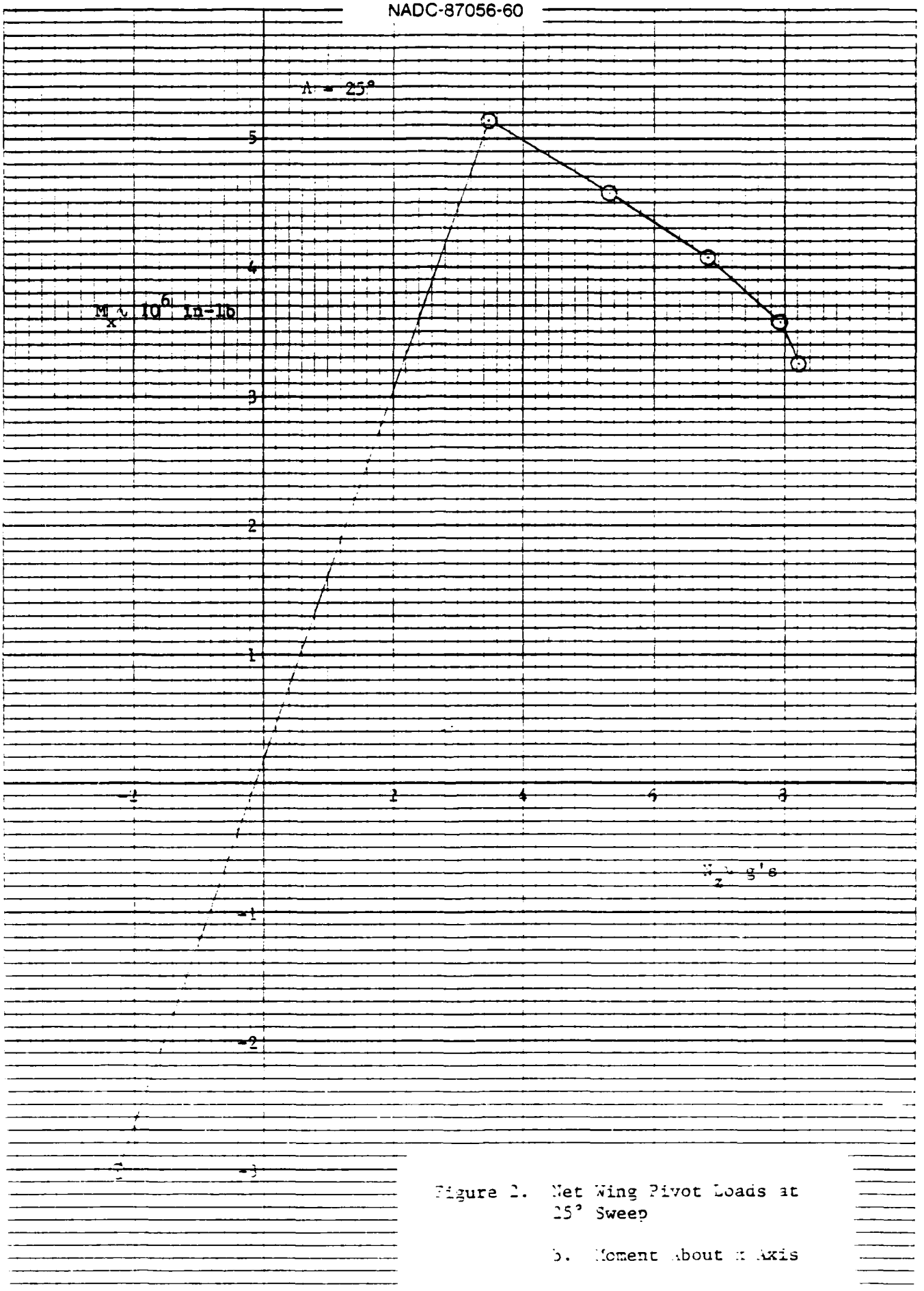


Figure 2. Net Wing Pivot Loads at 25° Sweep

b. Moment About X Axis

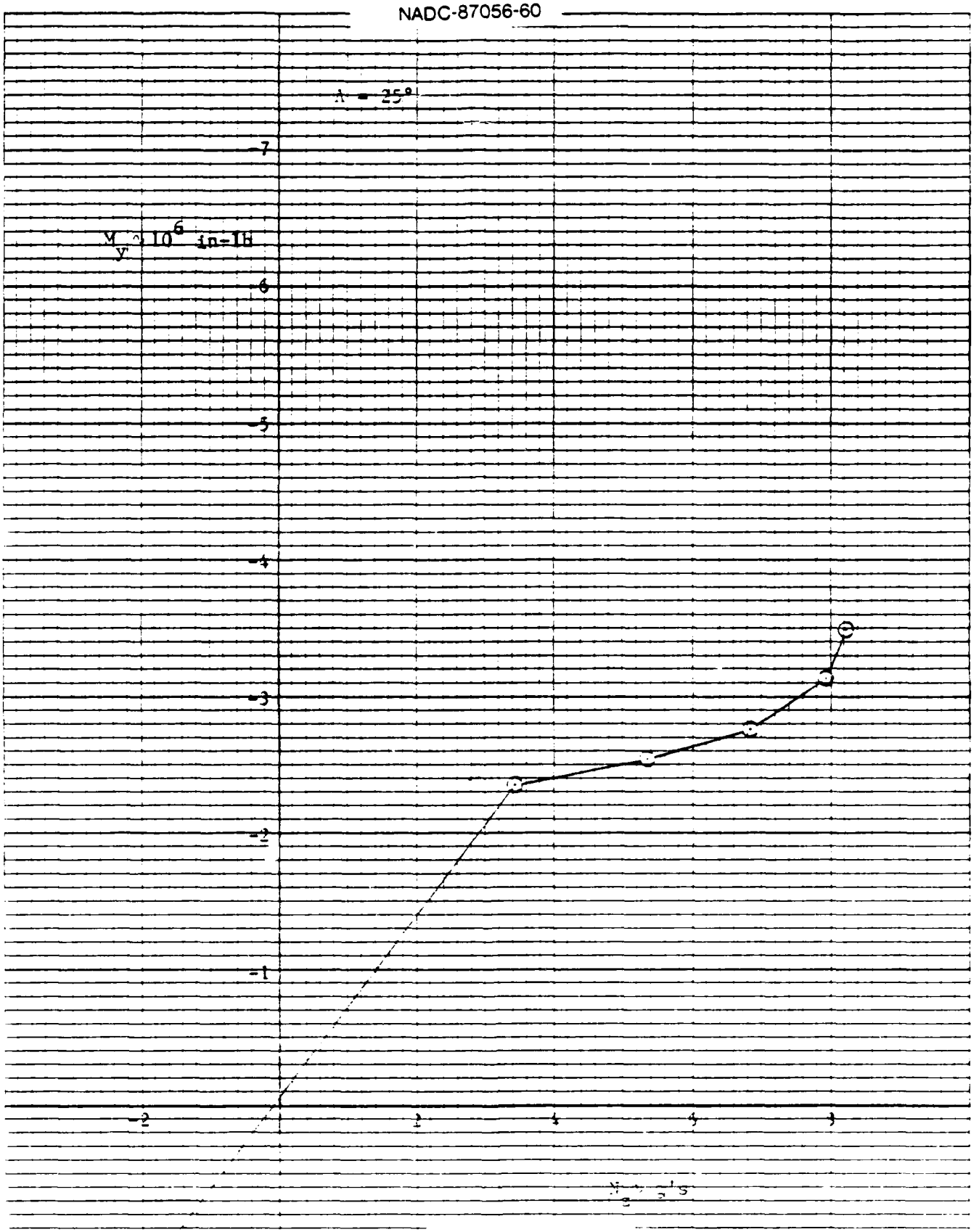


Figure 2. Net Wing Pivot Loads at 25° Sweep

a. Moment About y Axis

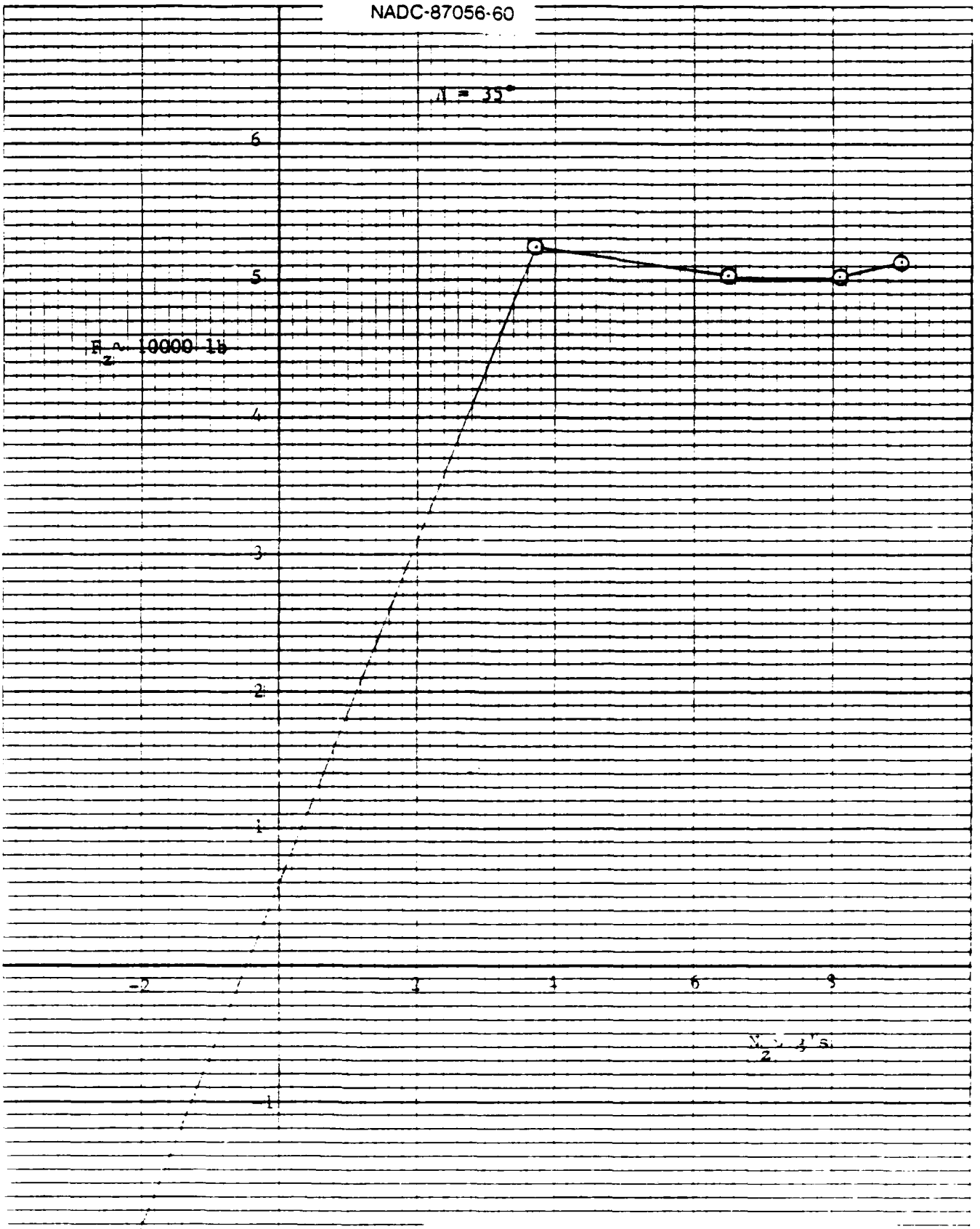


Figure 3. Net Wing Pivot Loads at 35° Sweep

a. Shear

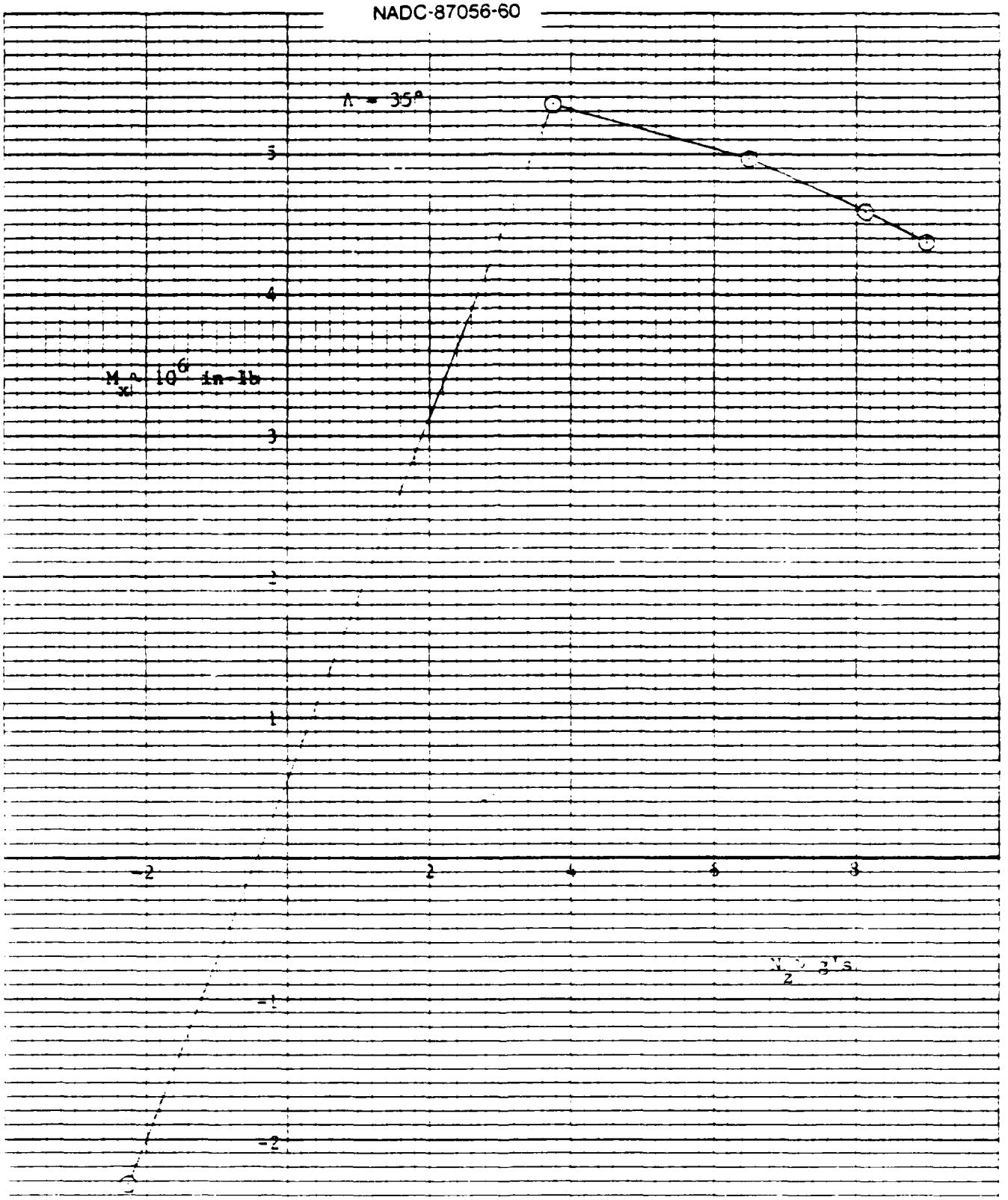


Figure 3. Net Wing Pivot Loads at 35° Sweep

b. Moment About x Axis

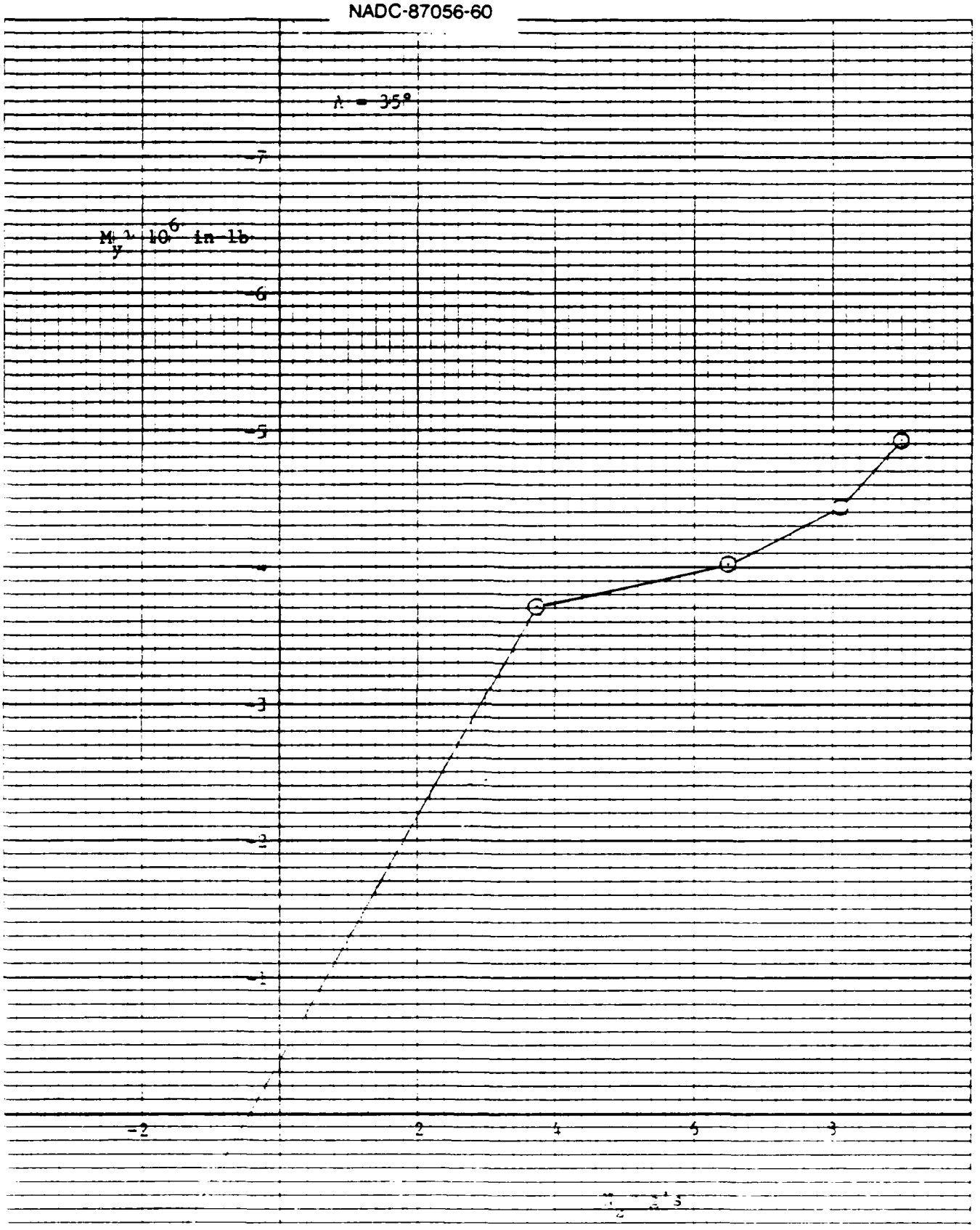


Figure 3. Net Wing Pivot Loads at 35° Sweep

a. Moment About Y Axis

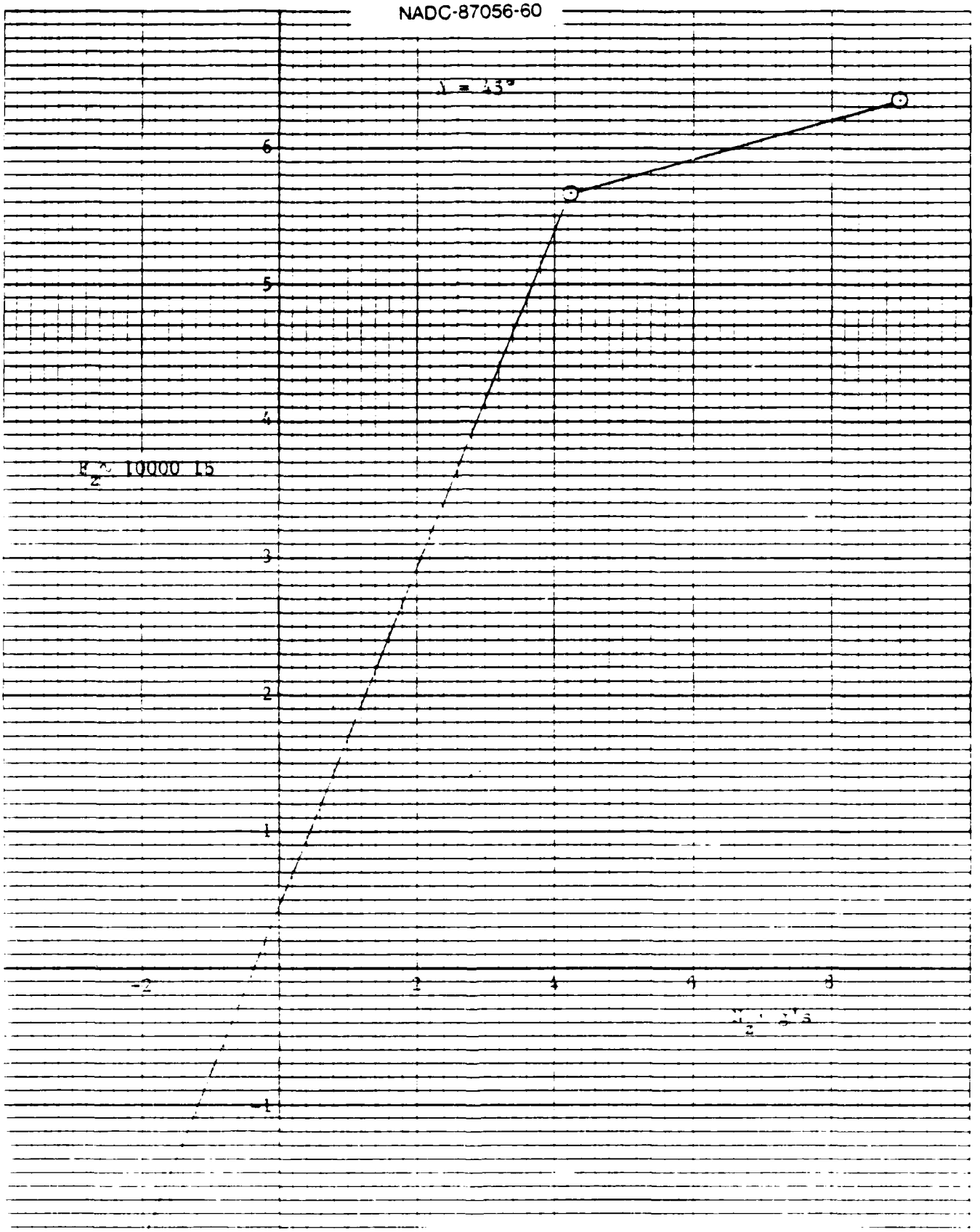


Figure 4. Net Wing Pivot Loads at 45° Sweep

a. Shear

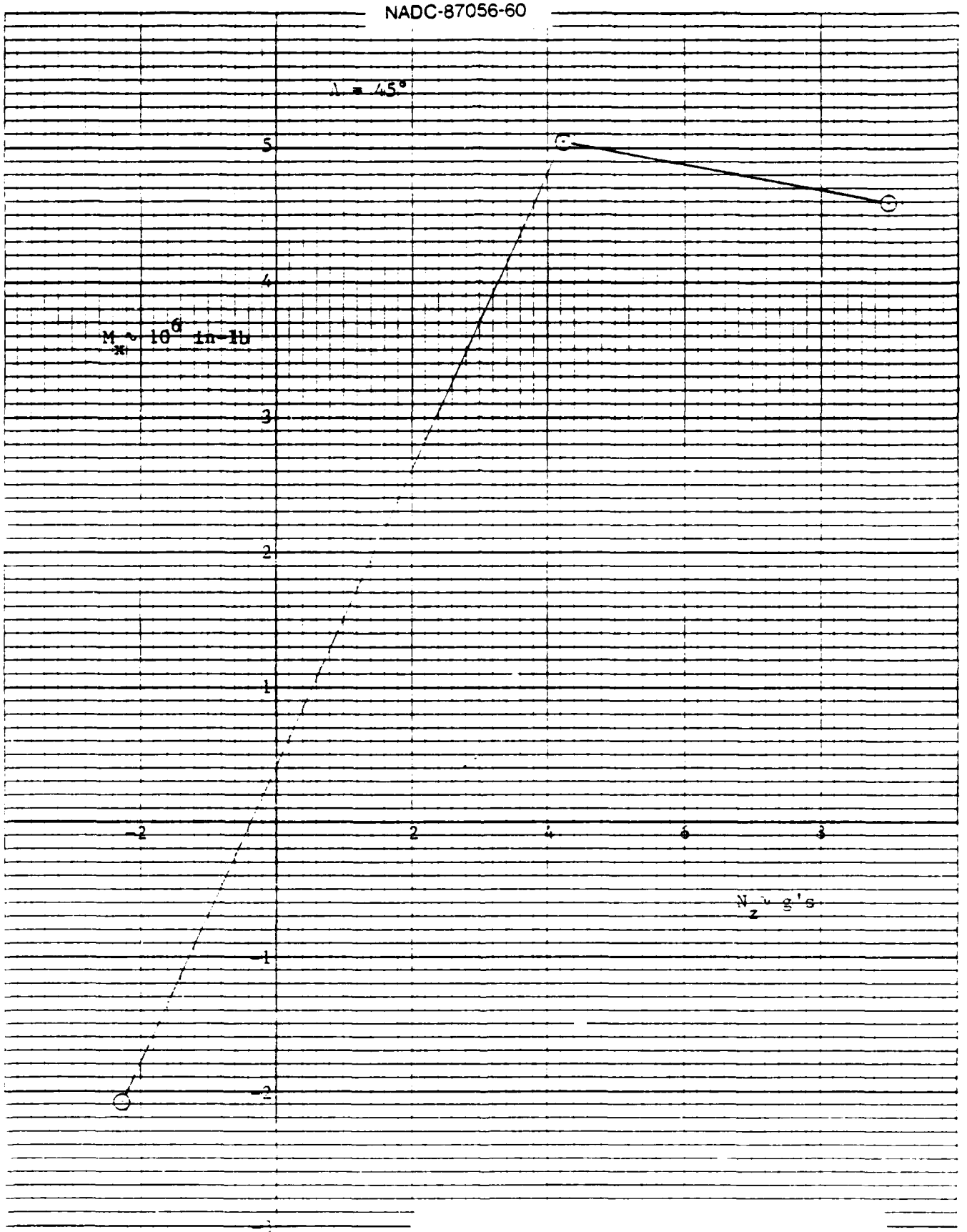


Figure 4. Net Wing Pivot Loads at 45° Sweep

b. Moment About X Axis

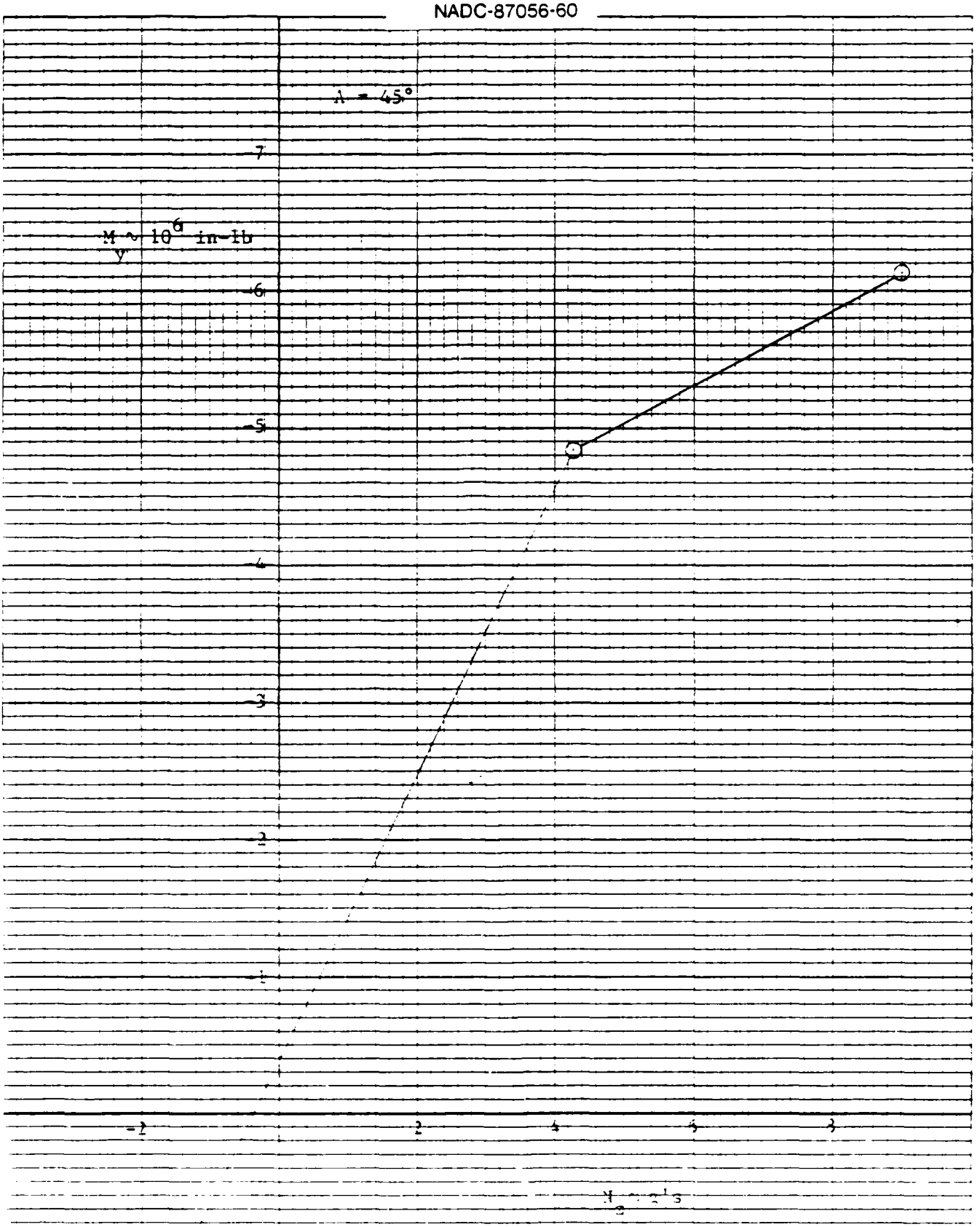


Figure 4. Net Wing Pivot Loads at 45° Sweep

a. Moment About y Axis

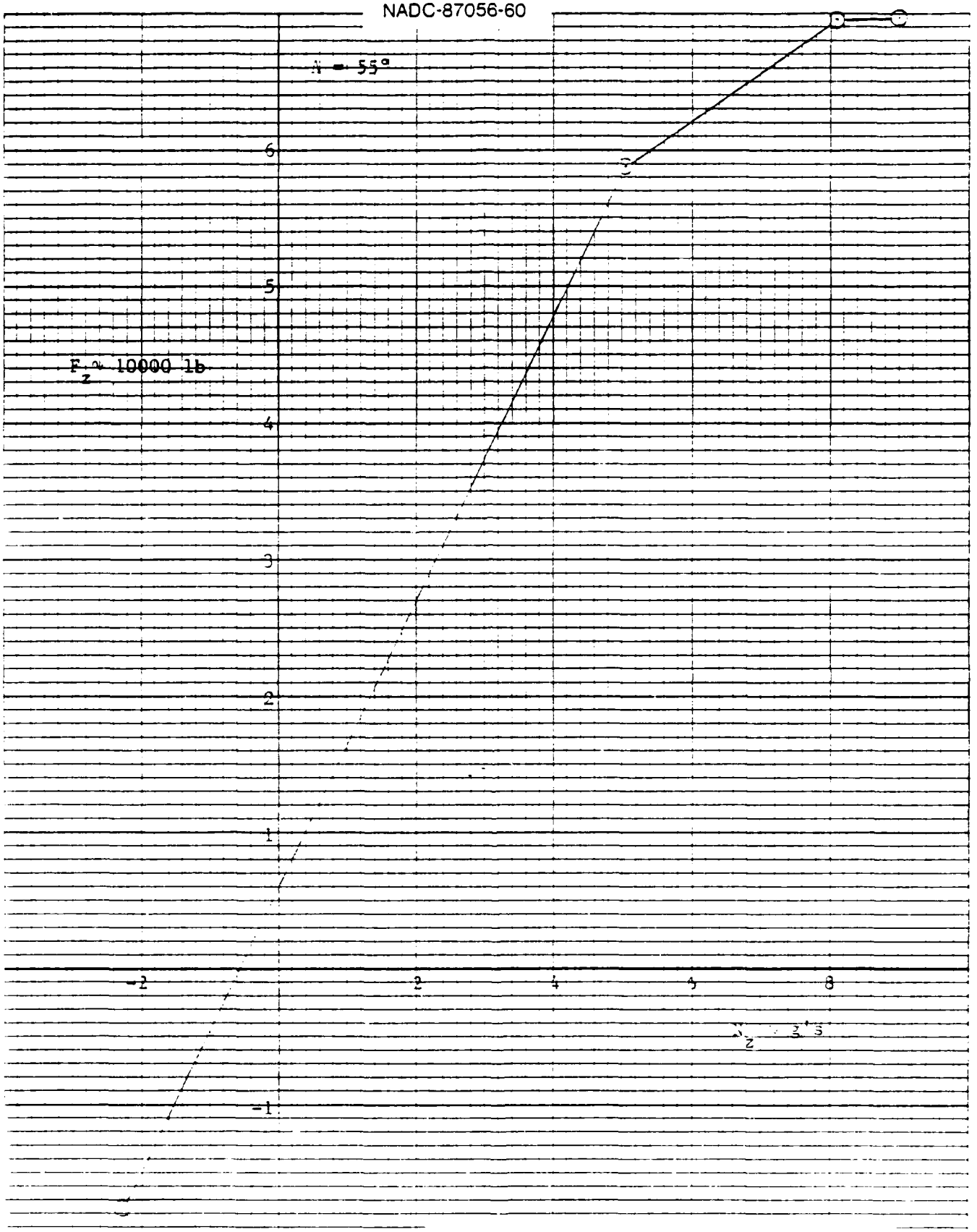


Figure 5. Net Wing Pivot Loads at 55° Sweep

1. Shear

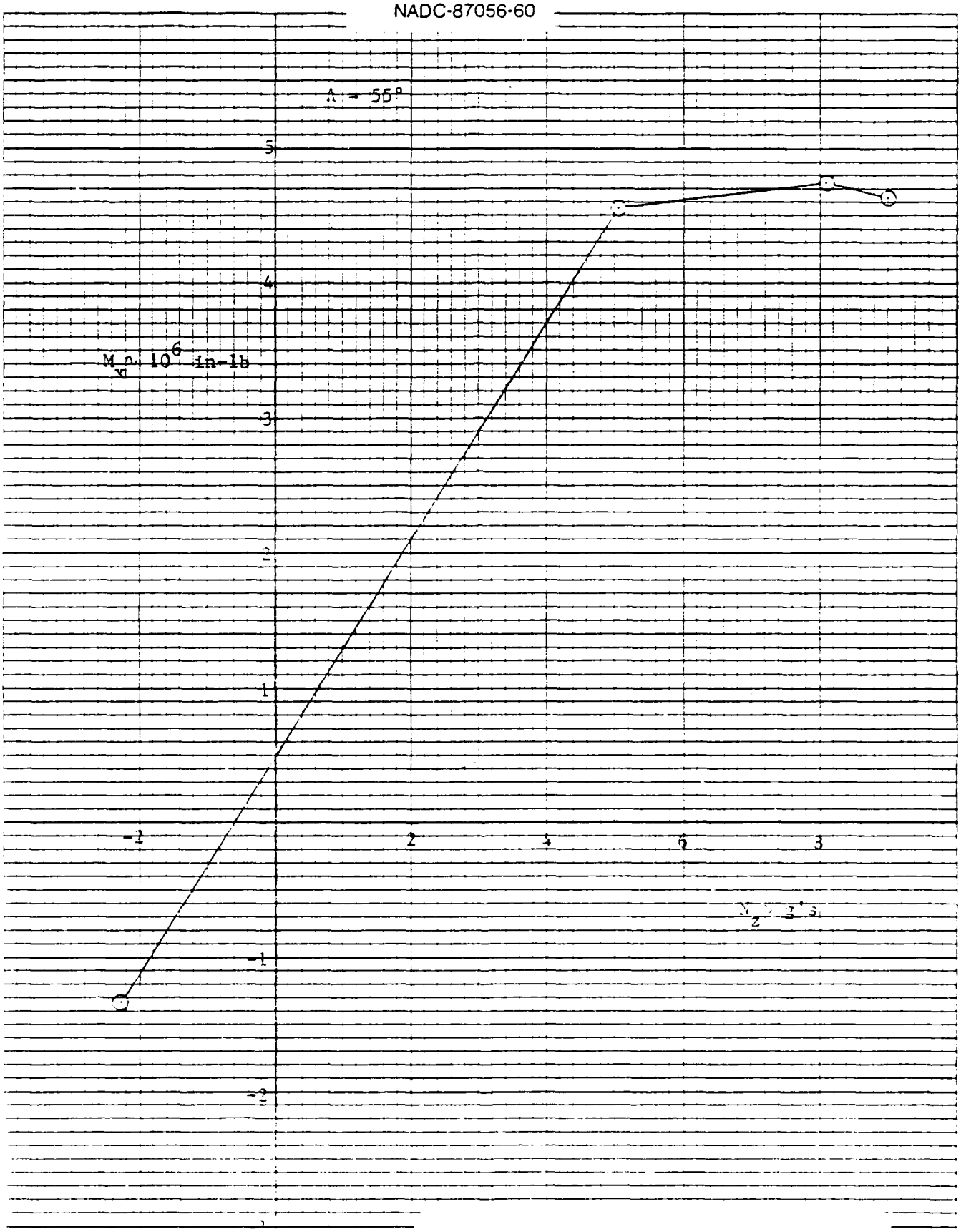


Figure 5. Net Wing Pivot Loads at 55° Sweep

b. Moment About x Axis

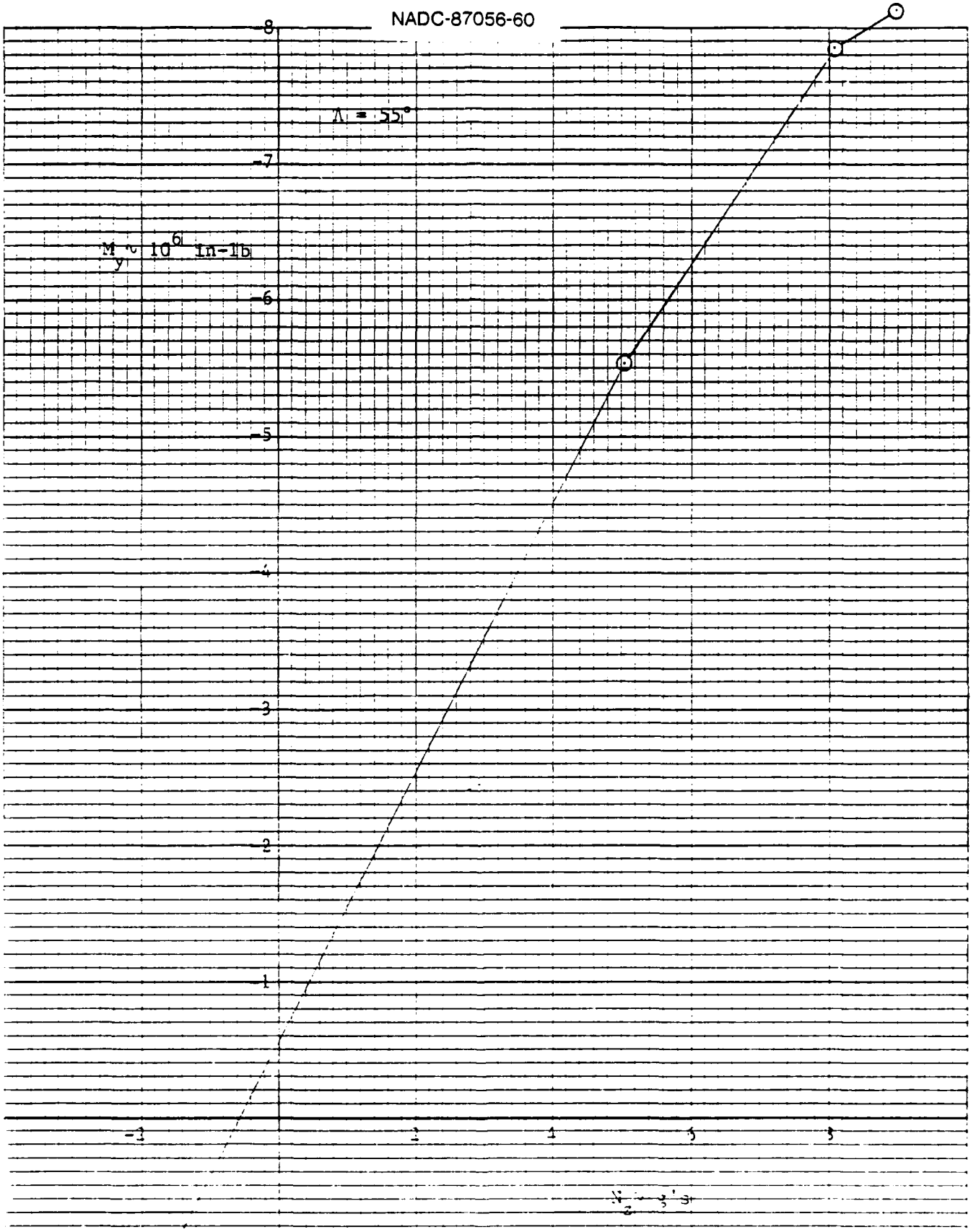


Figure 5. Net Wing Pivot Loads at 55° Sweep

c. Moment About y Axis

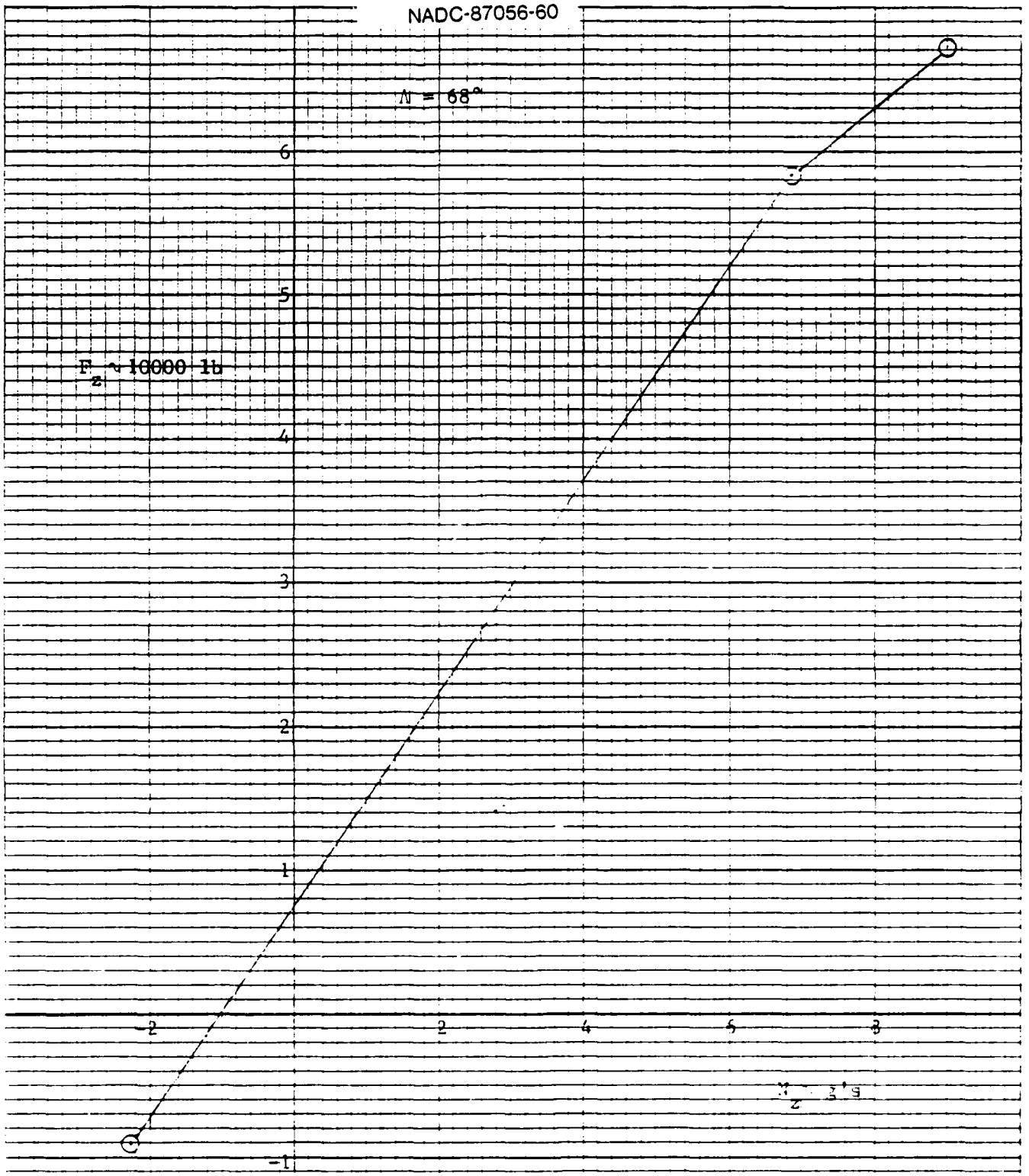


Figure 5. Net Wing Pivot Loads at 68° Sweep

a. Shear

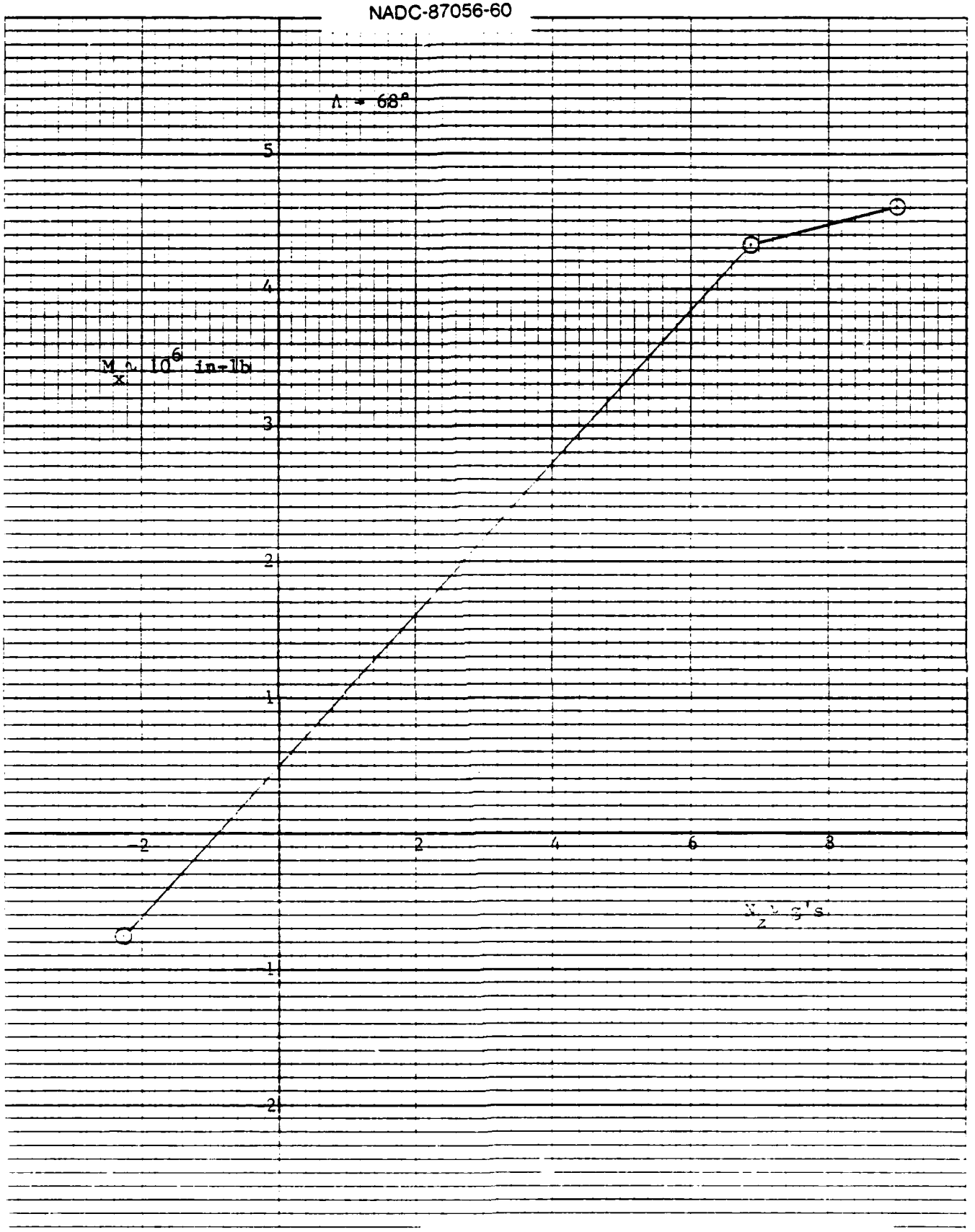


Figure 6. Net Wing Pivot Loads at 68° Sweep

b. Moment About x Axis

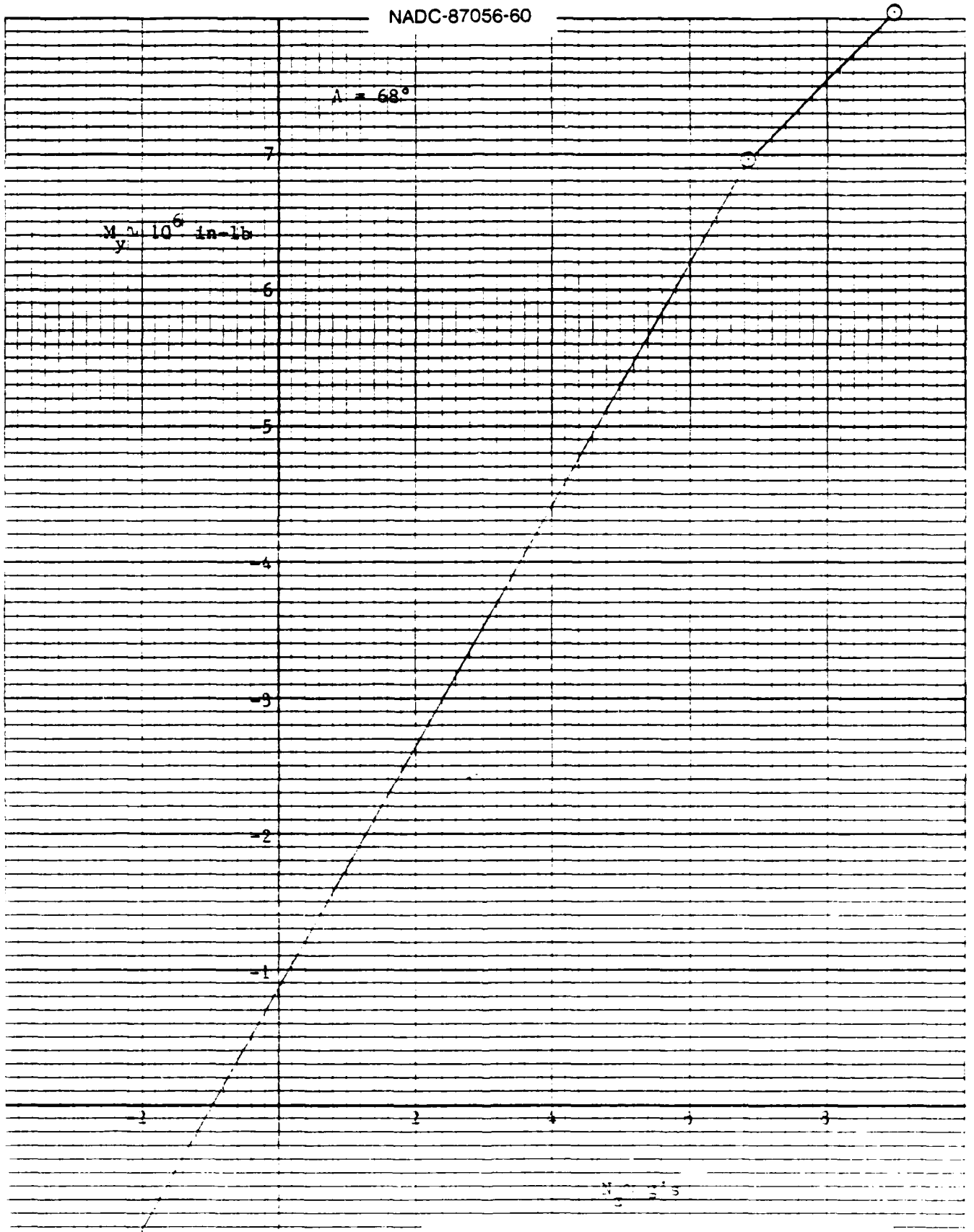


Figure 6. Net Wing Pivot Loads at 68° Sweep

c. Moment About y Axis

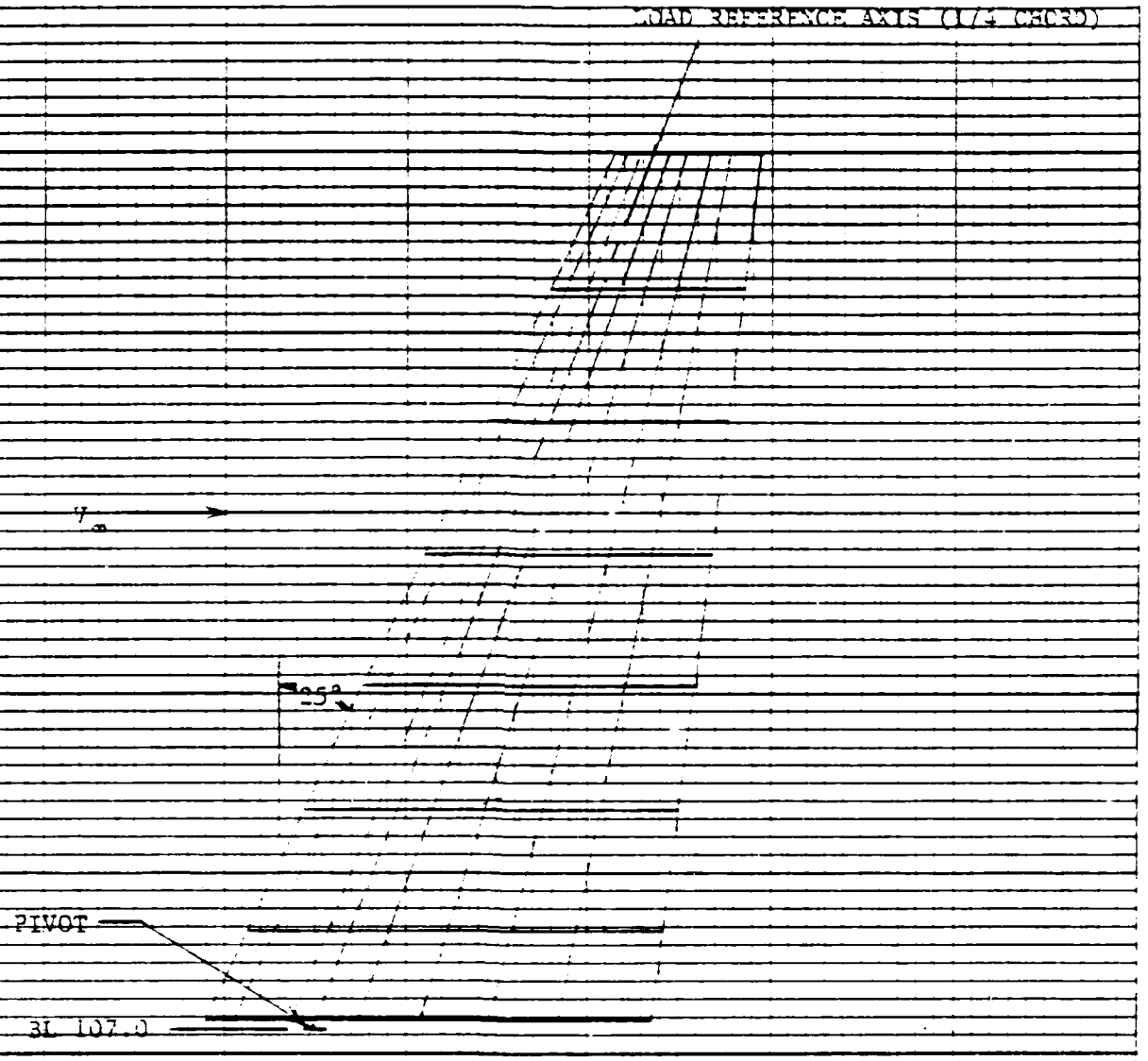


Figure 7. Aerodynamic Model of F-14 Wing Outer Panel

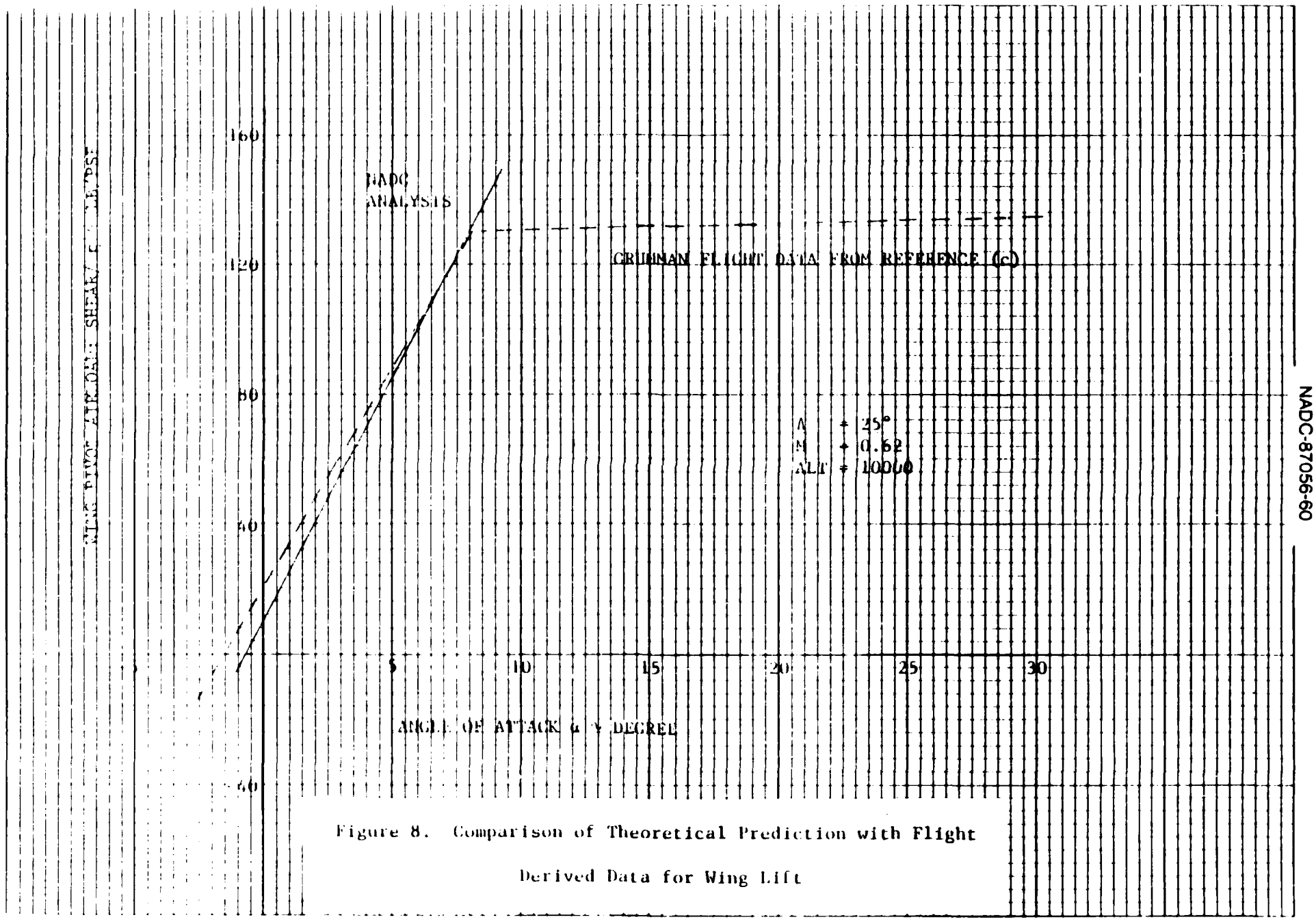


Figure 8. Comparison of Theoretical Prediction with Flight Derived Data for Wing Lift

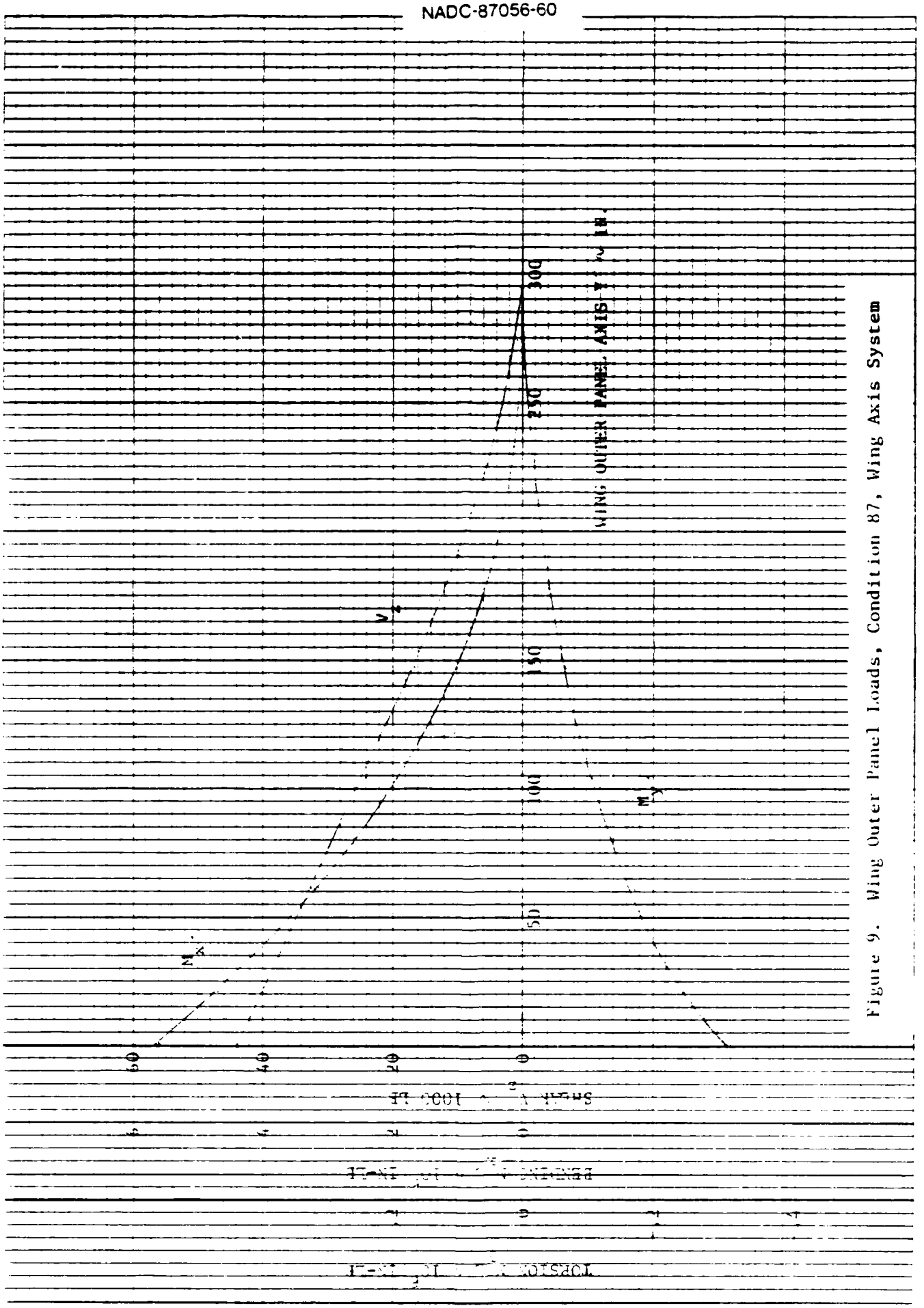


Figure 9. Wing Outer Panel Loads, Condition 87, Wing Axis System

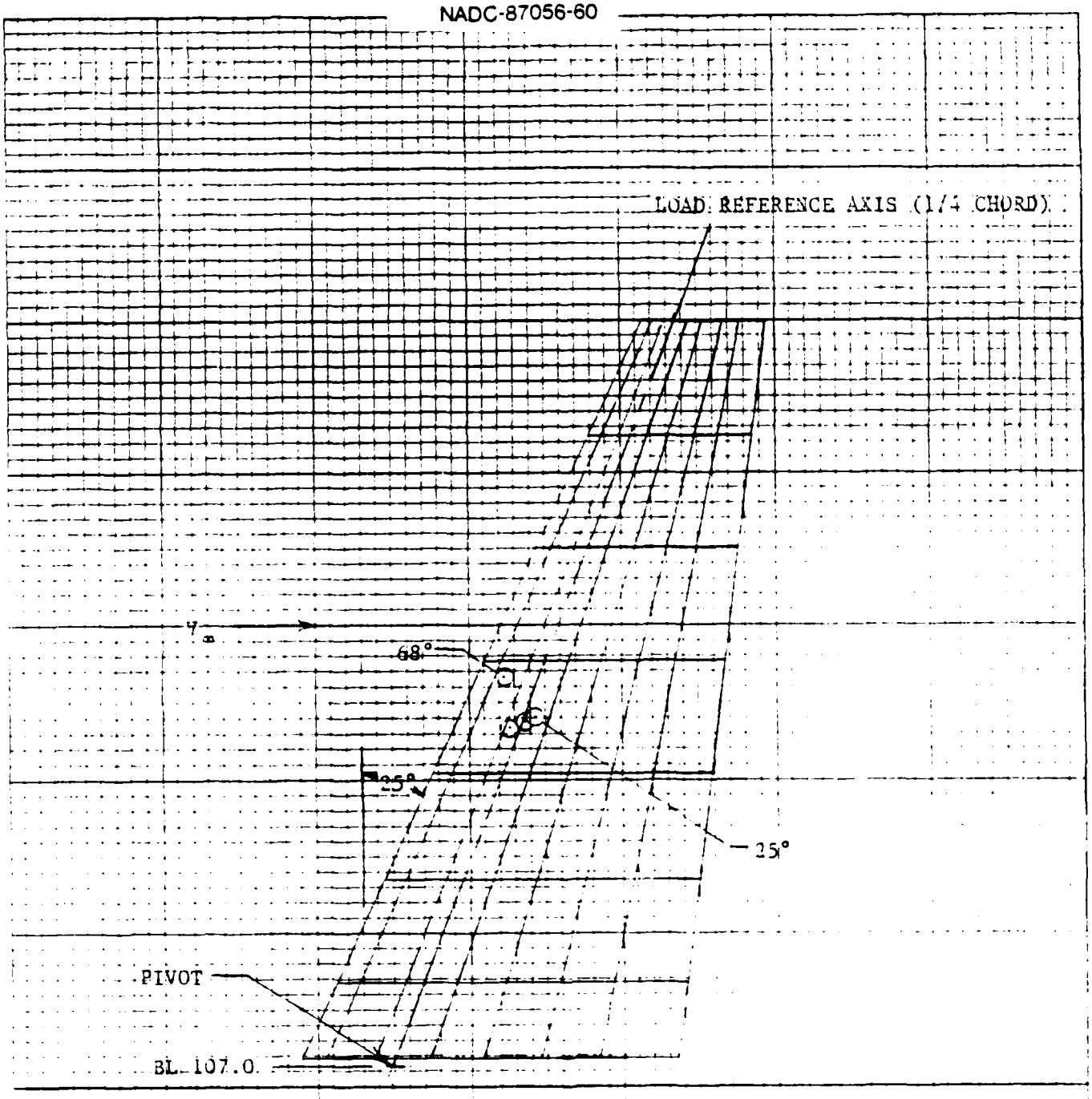


Figure 10. Wing Center of Pressure Location at Various Sweep Angles

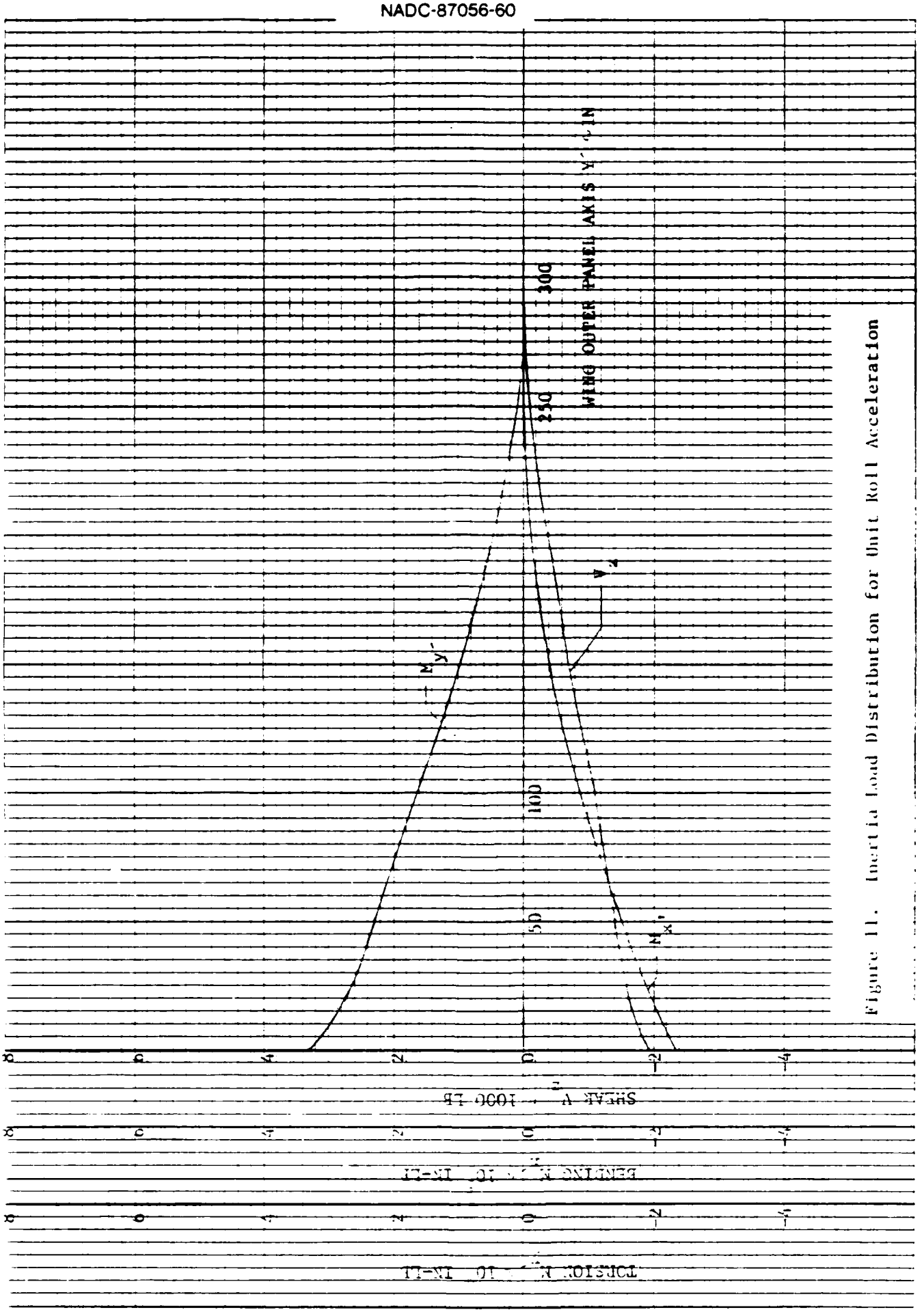


Figure 11. Inertia Load Distribution for Unit Roll Acceleration

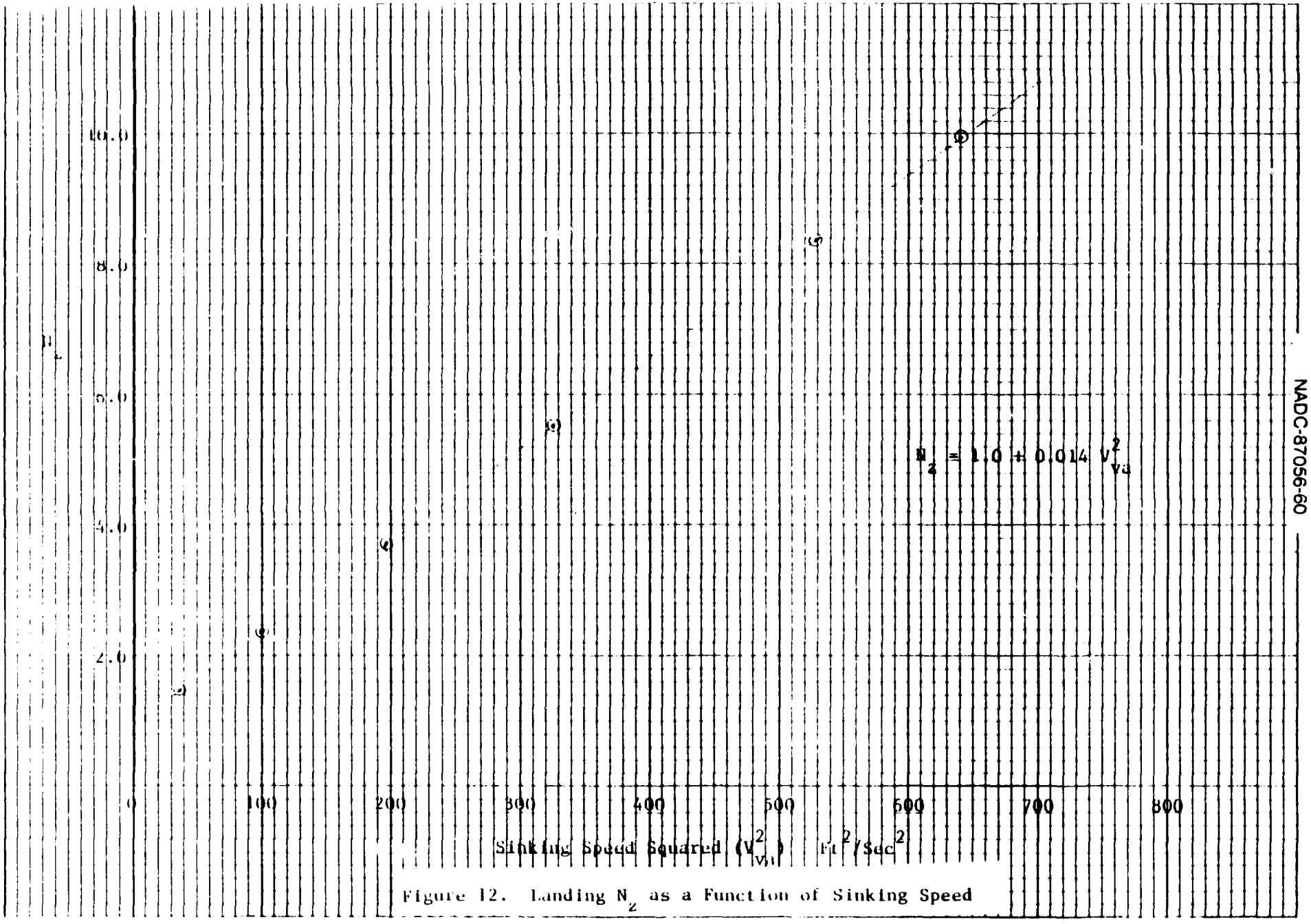


Figure 12. Landing N_z as a Function of Sinking Speed

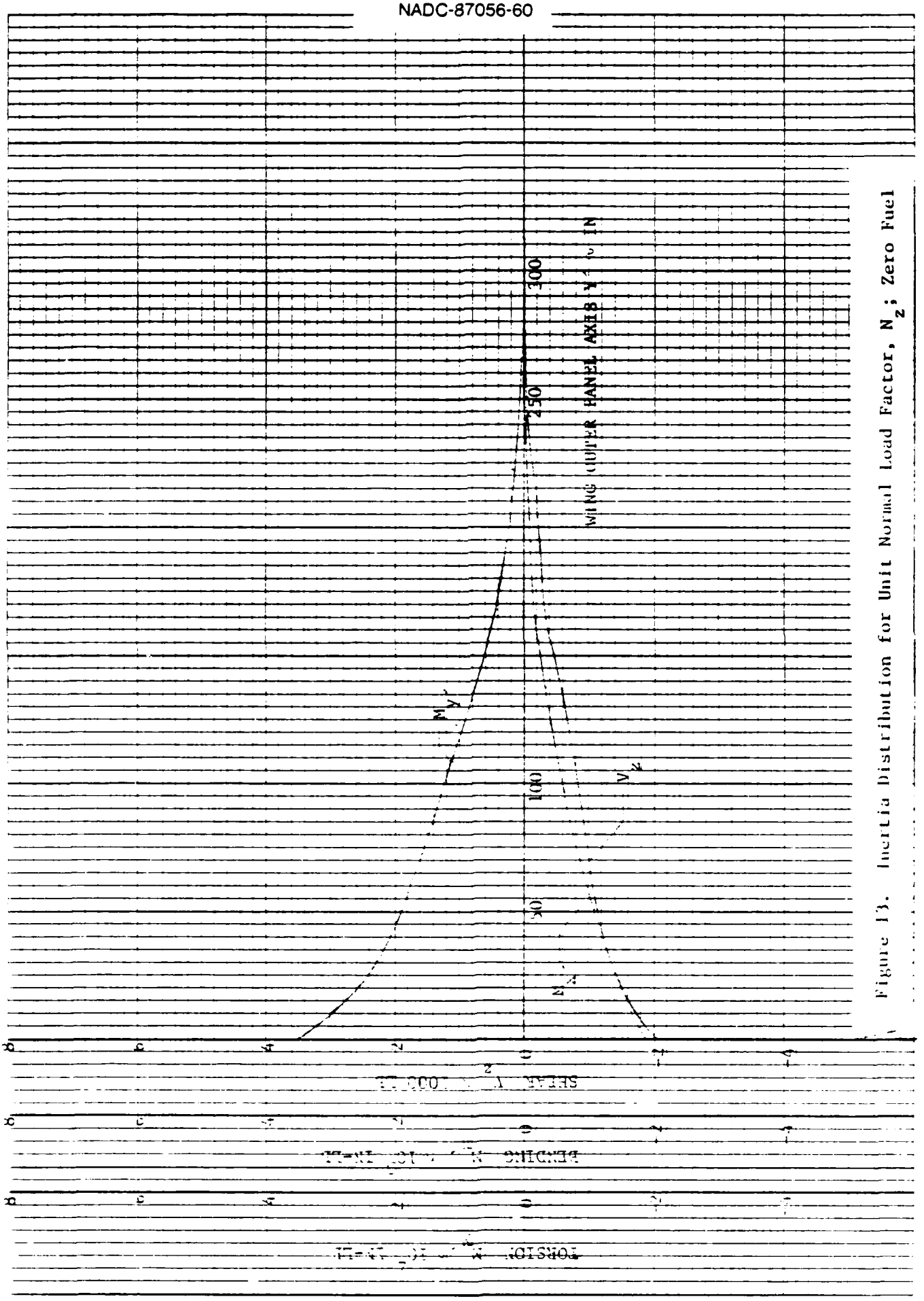


Figure 13. Inertia Distribution for Unit Normal Load Factor, N_Z; Zero Fuel

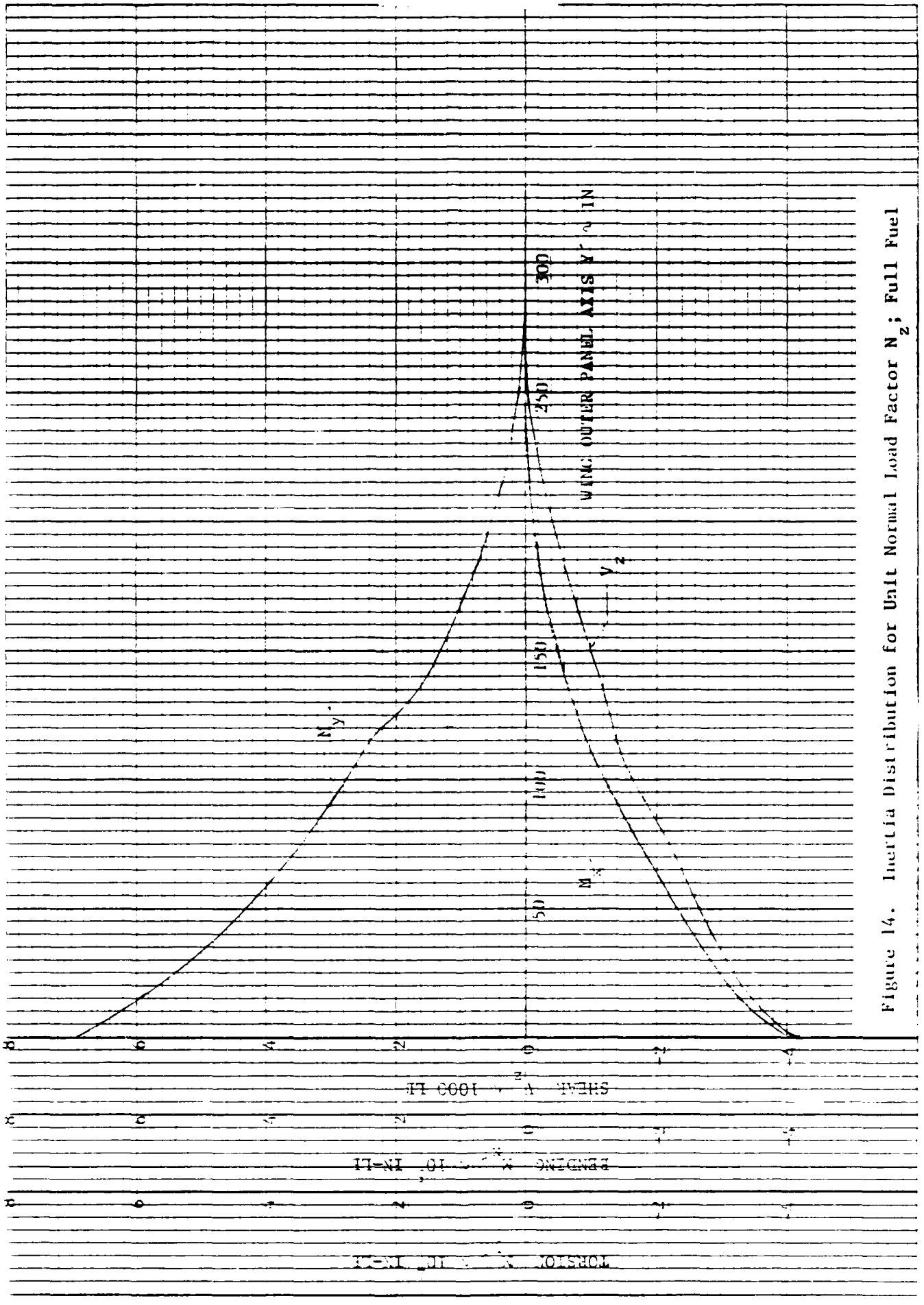


Figure 14. Inertia Distribution for Unit Normal Load Factor N_z; Full Fuel

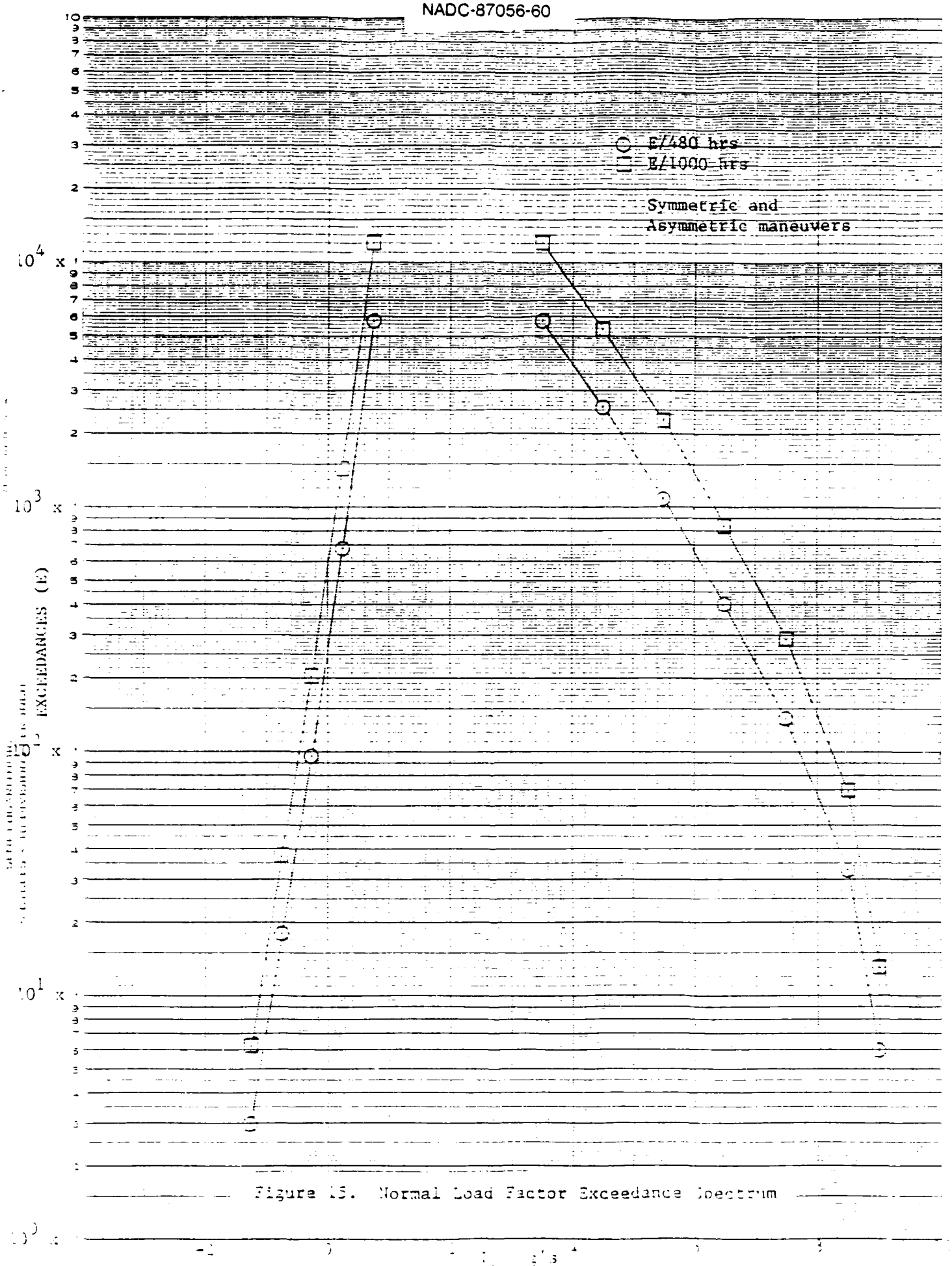
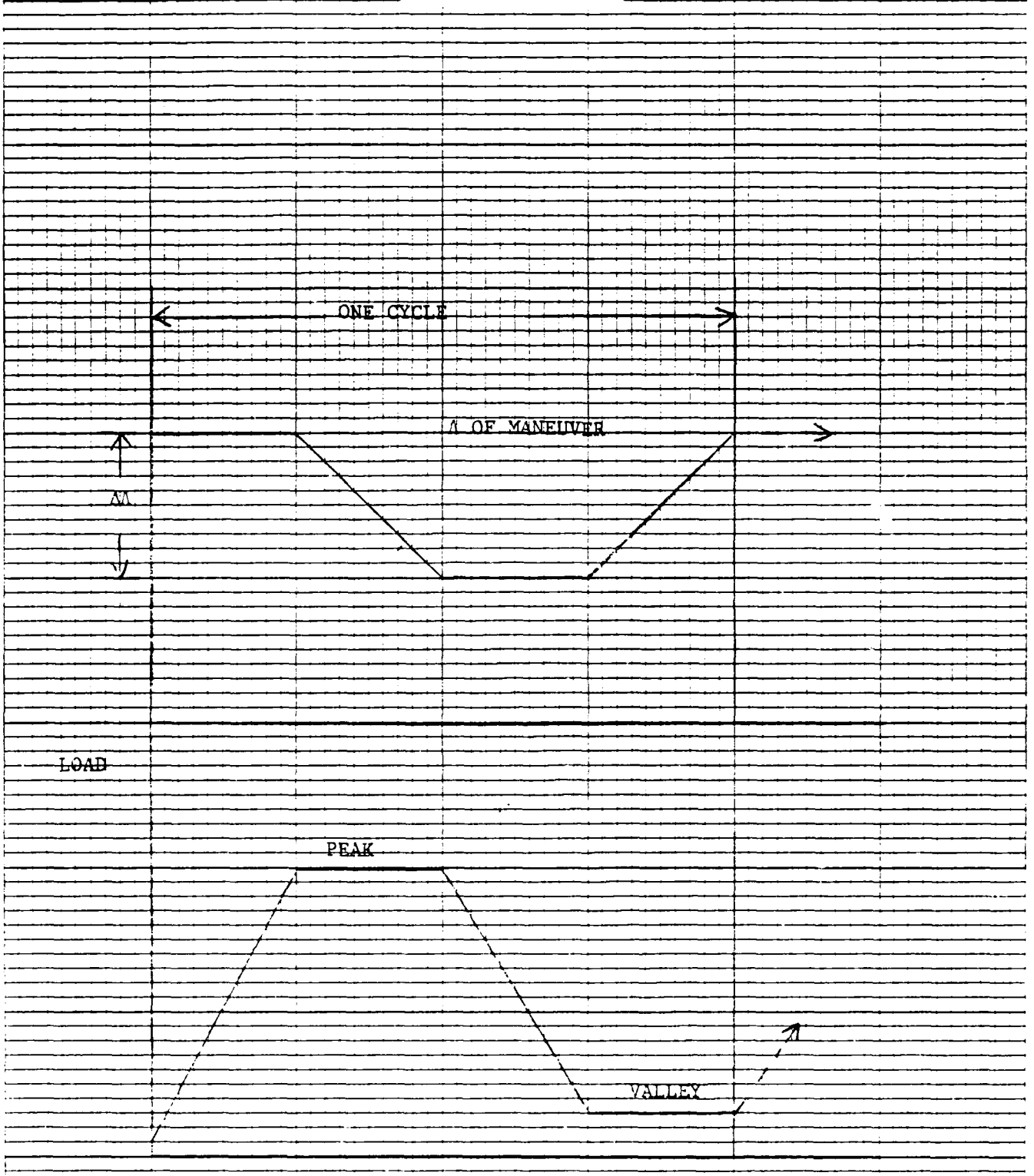


Figure 15. Normal Load Factor Exceedance Spectrum



Note: $\Delta\lambda$ = 5°, if λ_{LE} = 25° or if
650000 lb < bearing load < 650000 lb

$\Delta\lambda$ = 10° for any other λ_{LE} and if
bearing load ≤ 650000 lb

Figure 16. Wing Pivot Cycle

APPENDIX (A)

SEQUENTIAL SPECTRUM FOR AIRCRAFT #98 TEST

NOTE: Appendices (A) and (B) contain a flight-by-flight random sequence of load levels for 440 flights (480 hours). All printout lines (records) have the same format, which is described below:

Columns	Format	Description
1-4	I4	Flight number identification (1 to 440)
5-7	3X	Not used
8-9	I2	The number of loads in this line
10-69	20I3	These numbers identify the load conditions to be applied to the test article.

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1   20156156 87 87157155 87 87157155156156227228156156273274160155
1   20156156 87 87159155 87 87157155156156156156255256157155156156
1   20 87 87157155 87 87157155156156156156255256157155156156 87 87
1   20159155 87 87158155156156229230156156255256157154156156 87 87
1   16157155156156156156255256157155156156 38 39156156
2   20156156 87 87157155 87 87157155156156227228156156255256157155
2   20156156 87 87158155 87 87157155156156156156263264158155156156
2   20 87 87158155 87 87159155156156227228156156255256157155156156
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2   20 32 85156156148149156156 30 31 32 85156156148149156156 20 21
2    4 22 85156156
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    20157152 87 87158155156156156156261262158155156156 87 87157155
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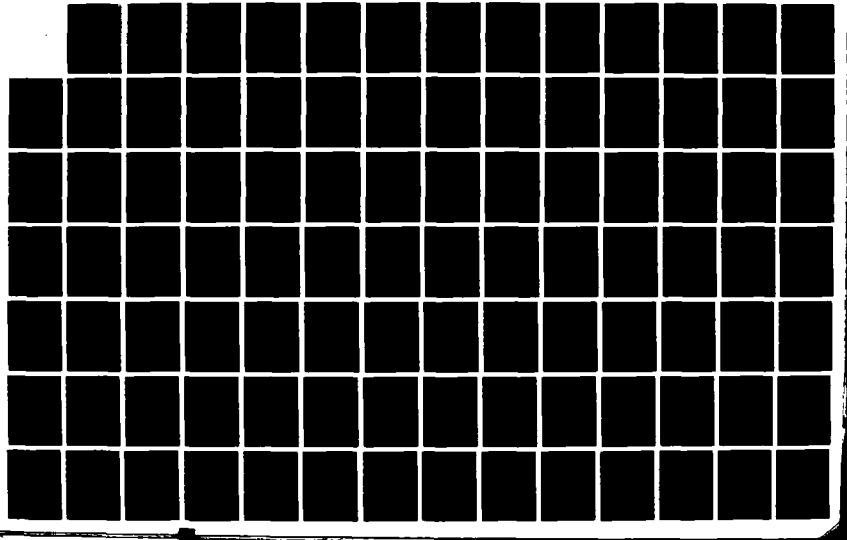
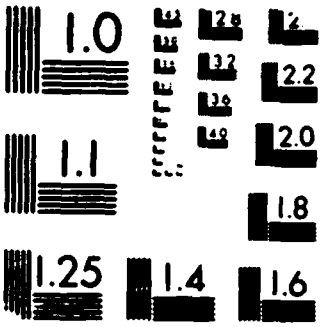
AD-A193 828 F-14 WING OUTER PANEL FATIGUE TEST SPECTRUM(U) NAVAL AIR DEVELOPMENT CENTER WARMINSTER PA AIR VEHICLE AND CREE SYSTEMS TECHN OLOGY DIRECTORATE G S SEIDEL ET AL. 2/3

UNCLASSIFIED APR 87 NADC-87056-60 F/G 1/3.3 NL





MICROCOPY RESOLUTION TEST CHART

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APPENDIX (B)

SEQUENTIAL SPECTRUM FOR WING OUTER PANEL TEST

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1   15159155 87158155156229230156255256157154156 87  0  0  0  0  0
1   10157155156255256157155156 20156  0  0  0  0  0  0  0  0  0  0
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2   13156 87158155 87157155156263264158155156  0  0  0  0  0  0  0
2   15 87158155 87159155156227228156255256157155156  0  0  0  0  0
2   13 87157155 87159155156255256157154156 87  0  0  0  0  0  0  0
2   11157155156255256157155156 17156  9  0  0  0  0  0  0  0  0  0
2   10 85156 20156  9 85156 20156 20  0  0  0  0  0  0  0  0  0  0
2    2 85156  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
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32    9171233234171  9156 17 85156  0  0  0  0  0  0  0  0  0  0  0
32    7  9156 [illegible]  9156 17  0  0  0  0  0  0  0  0  0  0  0  0  0
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33   11173170171 95173170171 17 85 62 85  0  0  0  0  0  0  0  0  0
33    3 84 74156  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
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36    1156  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
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41    6 85 62 85 84 72156  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
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42   111741701712802811721701711721701710  0  0  0  0  0  0  0  0  0
42    6 20 60 85 84 74156  0  0  0  0  0  0  0  0  0  0  0  0  0  0
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46  15 87157155 87157155156227228156261262158154156 0 0 0 0 0
46  11 87157153156255256157155156 17156 0 0 0 0 0 0 0 0 0
47  13156 87157155 87157155156261262158154156 0 0 0 0 0 0 0
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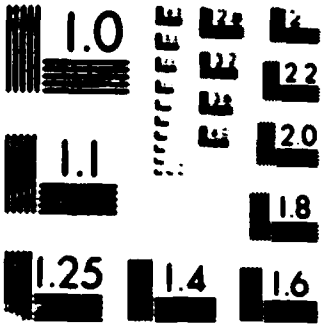
AD-A193 020 F-14 WING OUTER PANEL FATIQUE TEST SPECTRUM(U) NAVAL AIR DEVELOPMENT CENTER WARMINSTER PA AIR VEHICLE AND CREE SYSTEMS TECHN OLOGY DIRECTORATE G S SEIDEL ET AL. 3/3

UNCLASSIFIED APR 87 NADC-87056-60 F/G 1/3.3 NL



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322    3 17 85156  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0  0
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